

# Extreme violation of equipartition in mixtures

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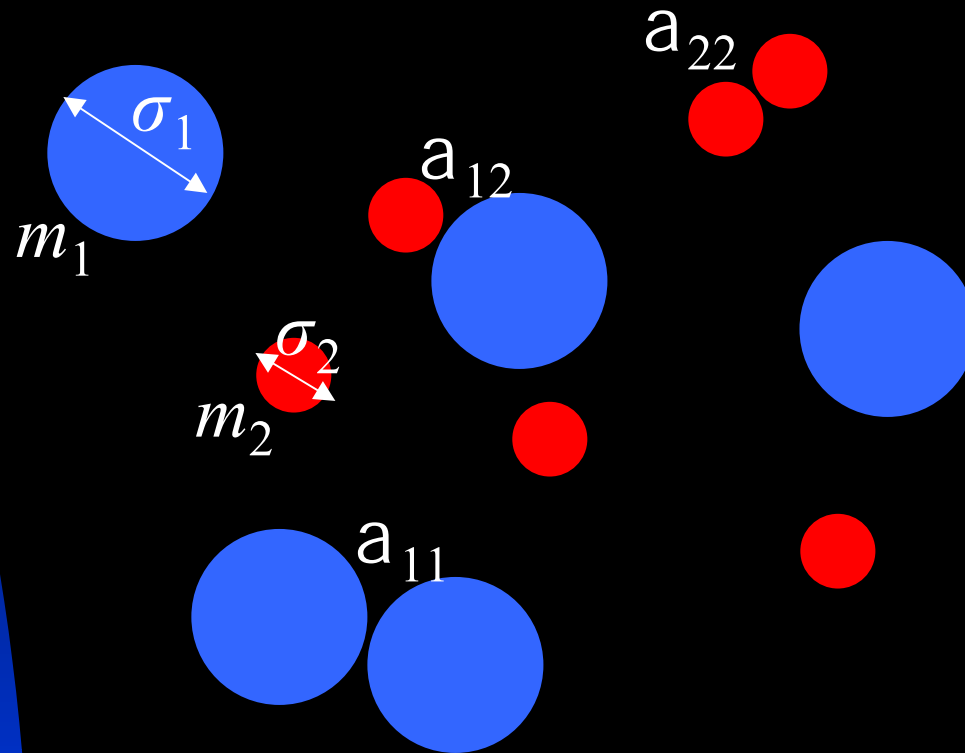


\* In collaboration with J.W. Dufty

# Outline

- Introduction (3-5)
- Kinetic theory description (6-8)
- Examples (9-13)
- Phase diagrams (14-24)
- Heated systems (25)
- Conclusions (26-27)

# Binary granular mixture



## Breakdown of Energy Equipartition in a 2D Binary Vibrated Granular Gas

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TABLE I. Some material properties of the spheres used in the experiment.

Particle	Mass [mg]	Effective inelasticity <sup>a</sup>	Mass ratio w/glass
Glass	5.24	0.17	—
Aluminum	5.80	0.31	0.92
Steel	15.80	0.21	0.33
Brass	18.00	0.39	0.28

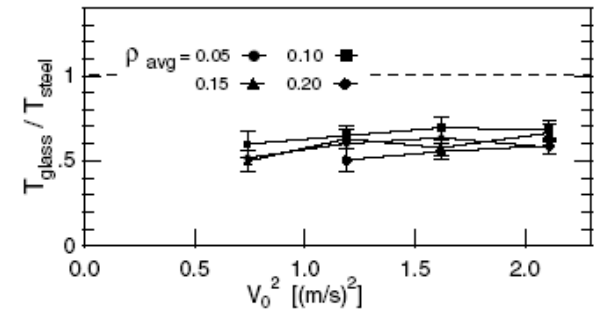


FIG. 4. Temperature ratio,  $\gamma = T_{\text{glass}}/T_{\text{steel}}$ , in a steel-glass mixture plotted against squared vibration velocity,  $v_0^2$ . Different markers represent different number densities of the mixture. The number fraction is fixed at  $x = 1/2$ . The horizontal dashed line represents equipartition ( $\gamma = 1$ ).

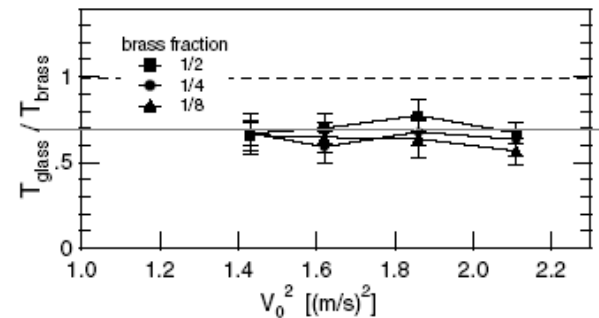


FIG. 5. Temperature ratio,  $\gamma = T_{\text{glass}}/T_{\text{brass}}$ , in a brass-glass mixture versus the squared vibration velocity of the cell,  $v_0^2$ . Different markers represent different number fractions of brass for the same total number of particles ( $\rho_{\text{avg}} = 0.049$ ). The horizontal dashed line represents equipartition ( $\gamma = 1$ ).

# Formulation of the problem

- Binary mixture of smooth inelastic hard spheres
  - ✓ Heavy species (1):  
 $m_1, \sigma_1, x_1 = n_1/n, a_{11}, a_{12}.$
  - ✓ Light species (2):  
 $m_2, \sigma_2, x_2 = n_2/n = 1 - x_1, a_{22}, a_{21} = a_{12}.$
- In the homogeneous cooling state,  
 $m_1 \hat{a} m_2 \hat{i} \quad , v_1^2 \hat{U}, v_2^2 \hat{U} \neq ?$

# Enskog-Boltzmann equation

$$\partial_t f_1(v) = J_{11}[f_1, f_1] + J_{12}[f_1, f_2]$$

$$\partial_t f_2(v) = J_{21}[f_2, f_1] + J_{22}[f_2, f_2]$$

$$\partial_t \langle v_1^2 \rangle = -\zeta_1 \langle v_1^2 \rangle, \quad \partial_t \langle v_2^2 \rangle = -\zeta_2 \langle v_2^2 \rangle$$

Rates of change  $\zeta_1 = \nu (\xi_{11} + \xi_{12}), \quad \zeta_2 = \nu (\xi_{21} + \xi_{22})$

Cooling rates

Thermalization rates

$$\nu = \frac{8\pi}{3} n g_{12} \sigma_{12}^2 \langle v_2 \rangle \frac{1 + \alpha_{12}}{2} \frac{m_2}{m_1 + m_2}$$

Effective collision frequency

# “Order” parameter

$$\phi \equiv \frac{\langle v_1^2 \rangle}{\langle v_2^2 \rangle}$$

$$\partial_t \phi = - (\zeta_1 - \zeta_2) \phi$$

Condition for HCS:

$$\zeta_1 = \zeta_2$$

# Maxwellian approximation

PHYSICAL REVIEW E

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Homogeneous cooling state for a granular mixture

Vicente Garzó\* and James Dufty

$$f_i(v) = n_i \left( \frac{m_i}{2\pi T_i} \right)^{3/2} \exp \left( -\frac{m_i v^2}{2T_i} \right), \quad \langle v_i^2 \rangle = \frac{3}{2} \frac{2T_i}{m_i}$$

$$h_2 \sim \frac{m_2}{m_1} \ll 1$$

$$\xi_{11}(\phi) \rightarrow x_1 \sqrt{\phi} \beta_1, \quad \xi_{12}(\phi) \rightarrow x_2 \sqrt{1 + \phi} \left( 1 - \frac{h_2}{\phi} \right),$$

**cooling rates**

**thermalization rates**

$$\xi_{22}(\phi) \rightarrow x_2 \beta_2, \quad \xi_{21}(\phi) \rightarrow x_1 \sqrt{1 + \phi} h_1^2 \left( 1 + \frac{\phi_0 - \phi}{h_2} \right)$$

$$\beta_1 \sim \frac{1 - \alpha_{11}^2}{h_2}, \quad \beta_2 \sim \frac{1 - \alpha_{22}^2}{h_2} \left( \frac{\sigma_2}{\sigma_1} \right)^2$$

$$\phi_0 = \frac{1 - \alpha_{12}}{1 + \alpha_{12}}, \quad h_1 = \frac{1 + \alpha_{12}}{2}$$

Elastic collisions:  $\phi = h_2^i$   $T_1/T_2 = 1$  Energy equipartition!

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# A few representative cases

- 1. Quasi-elastic cross collisions:

$$\alpha_{11} = \alpha_{22} = 1, \quad 1 - \alpha_{12} = O(h_2)$$

$$\beta_1 = \beta_2 = 0, \quad \phi_0 \sim h_2$$

$$\xi_{11}(\phi) = 0, \quad \xi_{12}(\phi) \rightarrow x_2 \left( 1 - \frac{h_2}{\phi} \right),$$

$$\xi_{22}(\phi) = 0, \quad \xi_{21}(\phi) \rightarrow x_1 \left( 1 + \frac{\phi_0 - \phi}{h_2} \right)$$

$$h_2 < \phi < h_2 + \phi_0$$

**Weak** breakdown of energy equipartition  
 $f \sim h_2, T_1 \sim T_2$

**“Normal” state**

- 2. Inelastic cross collisions:

$$\alpha_{11} = \alpha_{22} = 1, \quad 1 - \alpha_{12} = O(1)$$

$$\beta_1 = \beta_2 = 0, \quad \phi_0 \lesssim 1$$

$$\phi = \phi_0 = \frac{1 - \alpha_{12}}{1 + \alpha_{12}}$$

Regardless of the concentrations  $\hat{\nu}$

$$\xi_{11}(\phi) = 0, \quad \xi_{12}(\phi) \rightarrow x_2,$$

$$\xi_{22}(\phi) = 0, \quad \xi_{21}(\phi) \rightarrow x_1 \sqrt{1 + \phi} h_1^2 \frac{\phi_0 - \phi}{h_2}$$

{ No Brownian dynamics ( $x_1 \ddot{0} = 0$ )  
 No Lorentz gas ( $x_2 \ddot{0} = 0$ )

**Strong** breakdown of energy equipartition  
 $f \sim 1, T_1 / T_2 \ddot{0} \uparrow$

**“Ordered” state**

- 3. Inelastic heavy-heavy collisions:

$$\alpha_{12} = \alpha_{22} = 1, \quad 1 - \alpha_{11} = O(1)$$

$$\beta_2 = \phi_0 = 0, \quad \beta_1 \sim h_2^{-1}$$

$$\xi_{11}(\phi) \rightarrow x_1 \sqrt{\phi} \beta_1, \quad \xi_{12}(\phi) \rightarrow -x_2 \frac{h_2}{\phi}$$

$$\xi_{22}(\phi) = 0, \quad \xi_{21}(\phi) \rightarrow x_1$$

$$\phi \sim h_2^{4/3} \rightarrow 0, \quad T_1/T_2 \sim h_2^{1/3} \rightarrow 0$$

Again, **strong** breakdown of energy equipartition

“Sub-normal” state

- 4. Inelastic light-light collisions + disparate sizes:

$$\alpha_{11} = \alpha_{12} = 1, \quad 1 - \alpha_{22} = O(1), \quad S_i \sim m_i^{1/3}$$

$$\beta_1 = \phi_0 = 0, \quad \beta_2 \sim h_2^{-1/3}$$

$$\xi_{11}(\phi) = 0, \quad \xi_{12}(\phi) \rightarrow x_2$$

$$\xi_{22}(\phi) \rightarrow x_2 \beta_2, \quad \xi_{21}(\phi) \rightarrow -x_1 \frac{\phi}{h_2}$$

$$\phi \sim h_2^{2/3} \rightarrow 0, \quad T_1/T_2 \sim h_2^{-1/3} \rightarrow \infty$$

Intermediate between normal and ordered states

“Sub-ordered” (or “Super-normal”) state

- 5. Inelastic light-light collisions + Brownian limit:

$$\alpha_{11} = \alpha_{12} = 1, \quad 1 - \alpha_{22} = O(1), \quad x_1 = O(h_2)$$

$$\beta_1 = \phi_0 = 0, \quad \beta_2 \sim h_2^{-1}$$

$$\xi_{11}(\phi) = 0, \quad \xi_{12}(\phi) \rightarrow \phi^{1/2}$$

$$\xi_{22}(\phi) \rightarrow \beta_2, \quad \xi_{21}(\phi) \rightarrow -\frac{x_1}{h_2} \phi^{3/2}$$

$$\phi \sim h_2^{-2/3} \rightarrow \infty$$

**Very strong** breakdown of energy equipartition

“Super-ordered” state

# Classification of states

$$h_2 \sim \frac{m_2}{m_1}, \quad \phi = \frac{\langle v_1^2 \rangle}{\langle v_2^2 \rangle} \sim h_2^\eta, \quad \frac{T_1}{T_2} \sim h_2^{\eta-1}$$

State	$\eta$	$\langle v_1^2 \rangle / \langle v_2^2 \rangle$	$T_1 / T_2$	Example
Sub-normal	$\eta > 1$	0	0	$\alpha_{11} < 1$
Normal	$\eta = 1$	0	finite	$1 - \alpha_{12} \sim m_2 / m_1$
Sub-ordered	$0 < \eta < 1$	0	$\infty$	$\alpha_{12} < 1$
Ordered	$\eta = 0$	finite	$\infty$	$\alpha_{22} < 1, \sigma_i \sim m_i^{1/3}$
Super-ordered	$\eta < 0$	$\infty$	$\infty$	$\alpha_{22} < 1, x_1 \sim m_2 / m_1$

# Scaling laws

$$1 - \alpha_{11} \sim h_2^{a_1}, \quad (1 - \alpha_{22})(\sigma_2/\sigma_1)^2 \sim h_2^{a_2}, \quad 1 - \alpha_{12} \sim h_2^b$$

$a_1=0$  i Inelastic heavy-heavy collisions  
 $a_1=1$  i Elastic heavy-heavy collisions

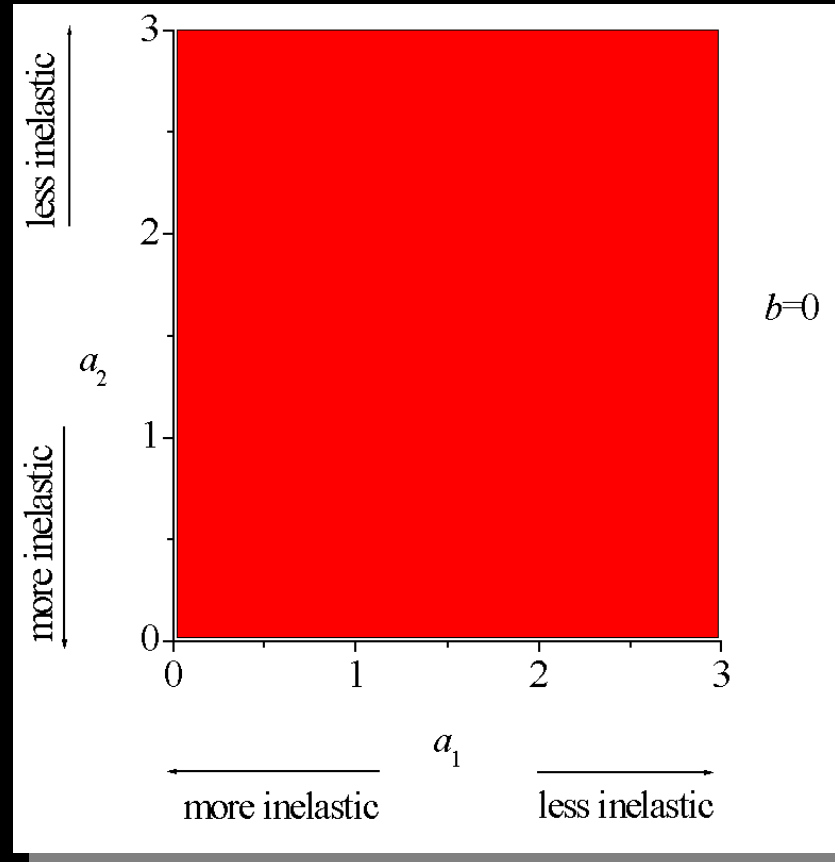
$b=0$  i Inelastic cross collisions  
 $b=1$  i Elastic cross collisions

$a_2=0$  i Inelastic light-light collisions + comparable sizes  
 $a_2=1$  i Elastic light-light collisions

$$\phi \sim h_2^\eta, \quad \eta \stackrel{?}{=} \eta(a_1, a_2, b)$$

# Phase diagram (finite concentrations)

Inelastic cross collisions



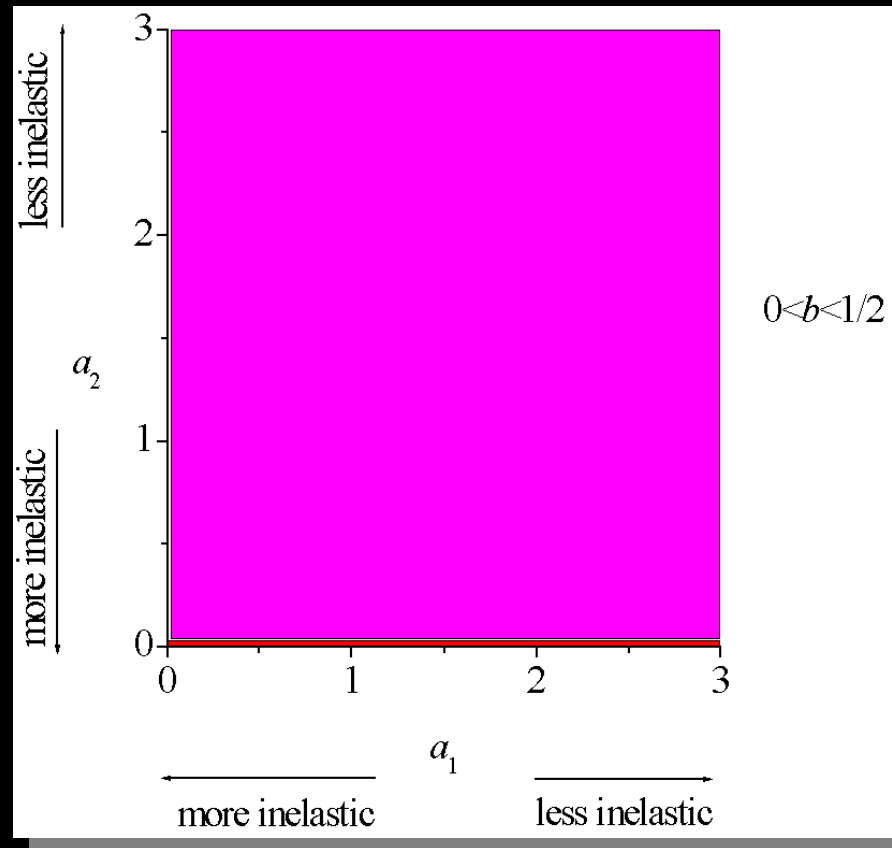
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# Phase diagram (finite concentrations)

Weakly quasi-elastic cross collisions

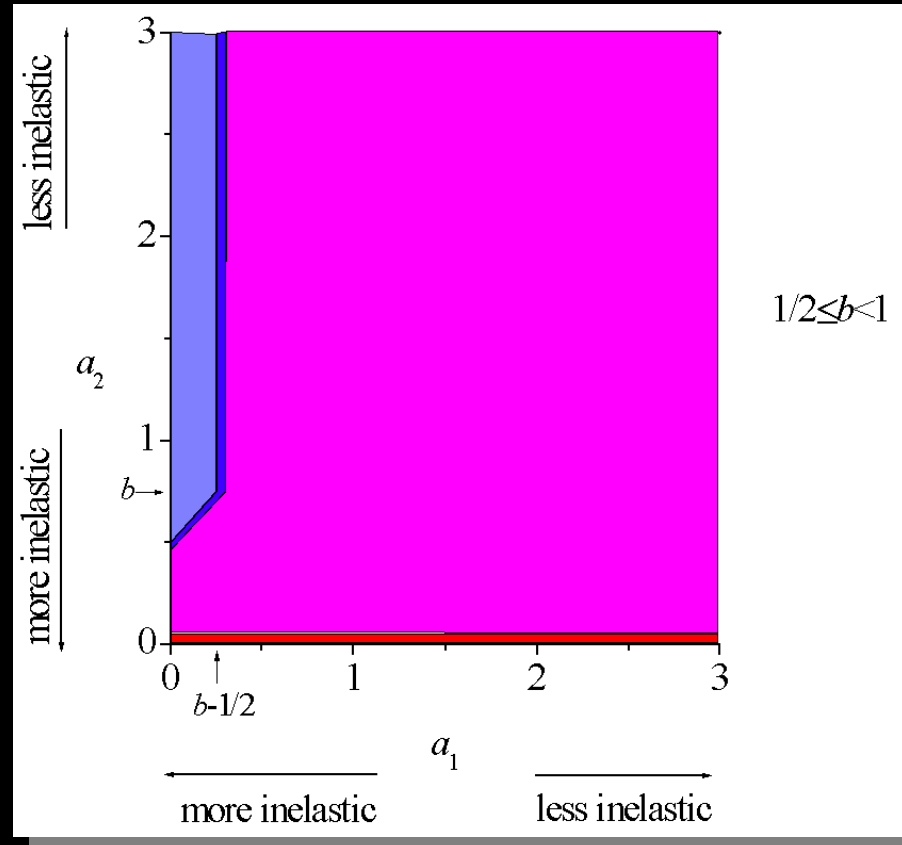


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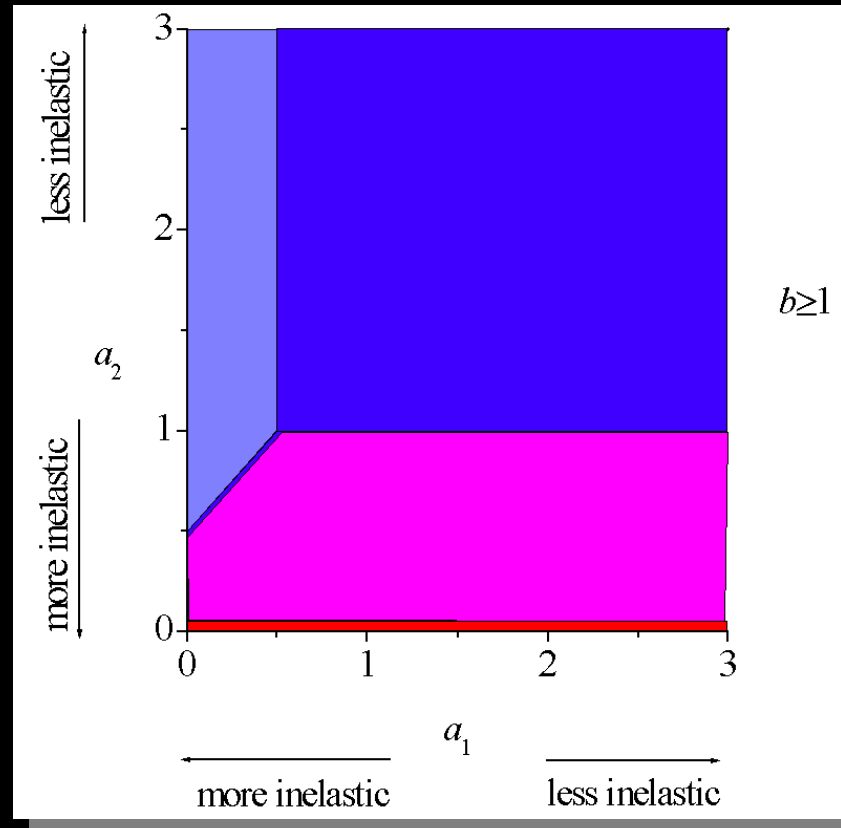
# Phase diagram (finite concentrations)

## Quasi-elastic cross collisions



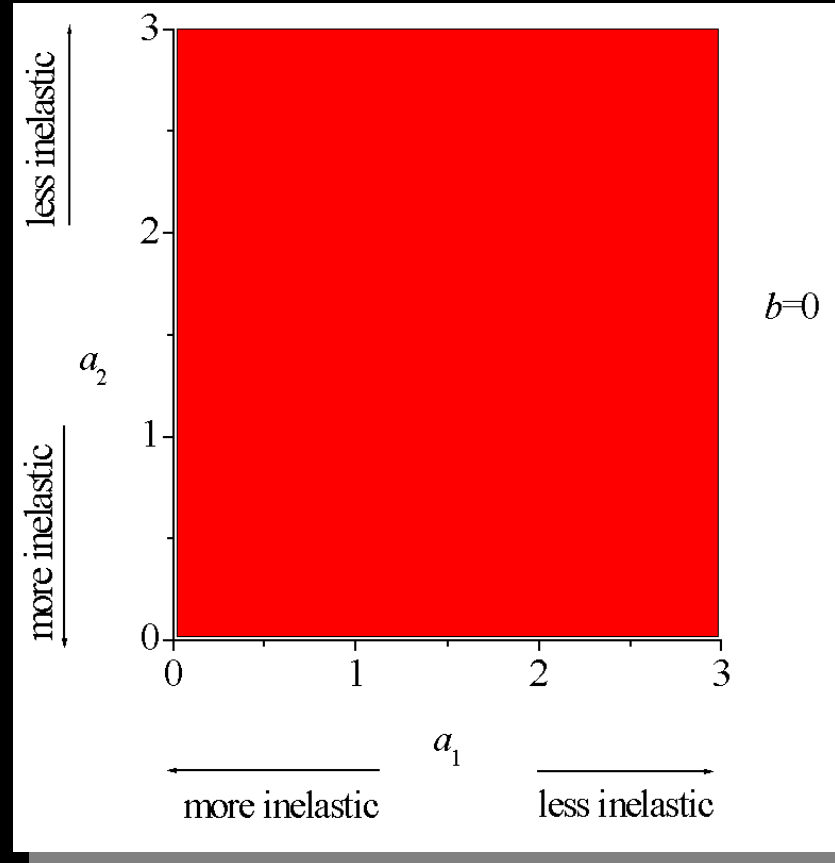
# Phase diagram (finite concentrations)

Strongly quasi-elastic cross collisions



# Phase diagram (finite concentrations)

Inelastic cross collisions



$$1 - \alpha_{12} = \mathcal{O}(1)$$

$$1 - \alpha_{11} \sim h_2^{a_1}$$

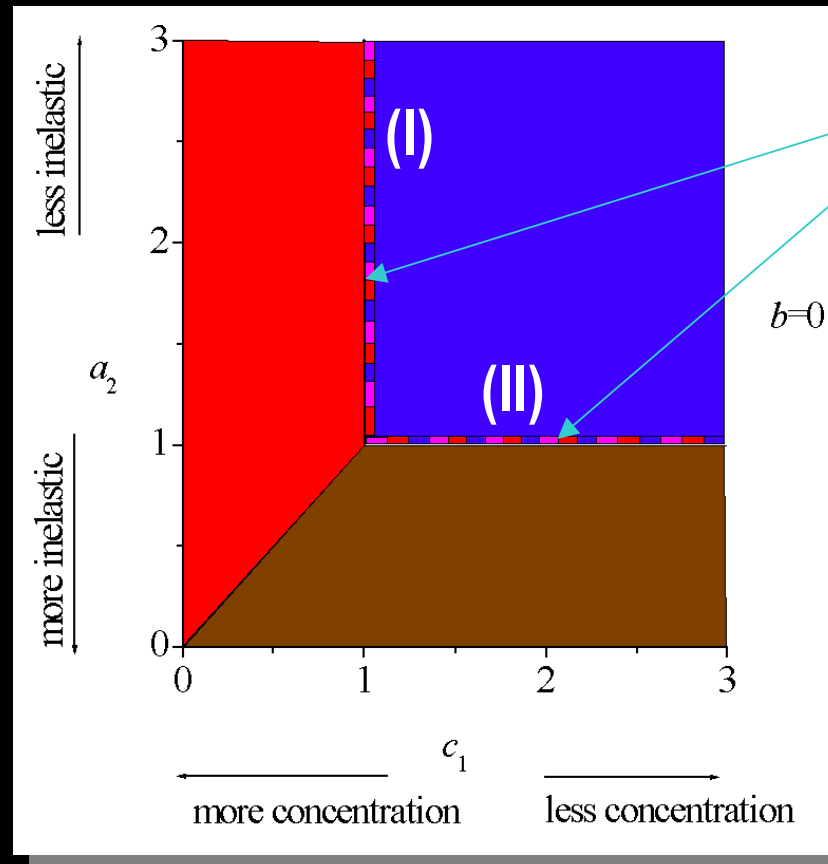
$$(1 - \alpha_{22})(\sigma_2/\sigma_1)^2 \sim h_2^{a_2}$$

$$x_1 \sim h_2^{c_1}$$

# Phase diagram (Brownian limit)

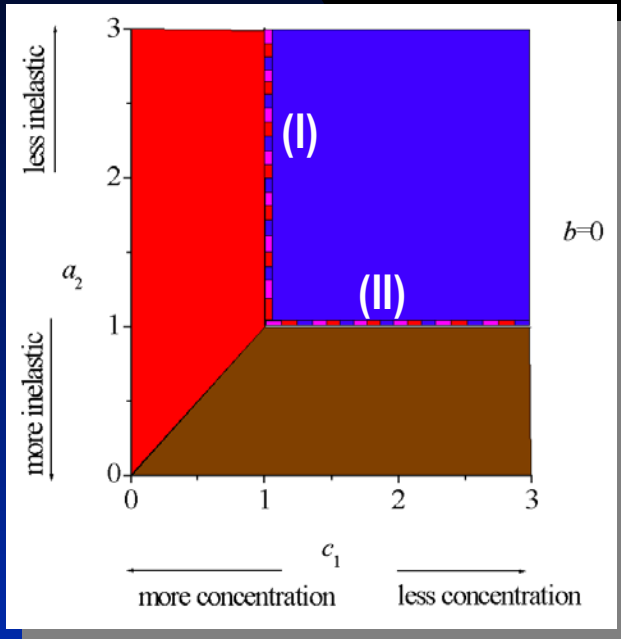
Inelastic cross collisions

Sub-normal	
Normal	
Sub-ordered	
Ordered	
Super-ordered	



# Critical lines (Brownian limit)

$$(I) x_1 \sim h_2, b_2 \ddot{O} 0$$



$$\frac{x_1}{h_2} \frac{1 - \alpha_{12}^2}{4} \begin{cases} < 1 \Rightarrow \phi \sim h_2 \\ = 1 \Rightarrow \phi \sim h_2^{1/2} \\ > 1 \Rightarrow \phi \sim 1 \end{cases}$$

- normal
- sub-ordered
- ordered

$$(II) 1 - a_{22} \sim h_2, x_1/h_2 \ddot{O} 0$$

$$\beta_2 \begin{cases} < 1 \Rightarrow \phi \sim h_2 \\ = 1 \Rightarrow \phi \sim h_2^{1/2} \\ > 1 \Rightarrow \phi \sim 1 \end{cases}$$

- normal
- sub-ordered
- ordered

# Case (II) $1 - a_{22} \sim h_2, x_1/h_2 \ddot{O} 0$

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## Critical Behavior of a Heavy Particle in a Granular Fluid

Andrés Santos\* and James W. Dufty†

PHYSICAL REVIEW E, VOLUME 64, 051305

## Nonequilibrium phase transition for a heavy particle in a granular fluid

Andrés Santos\* and James W. Dufty†

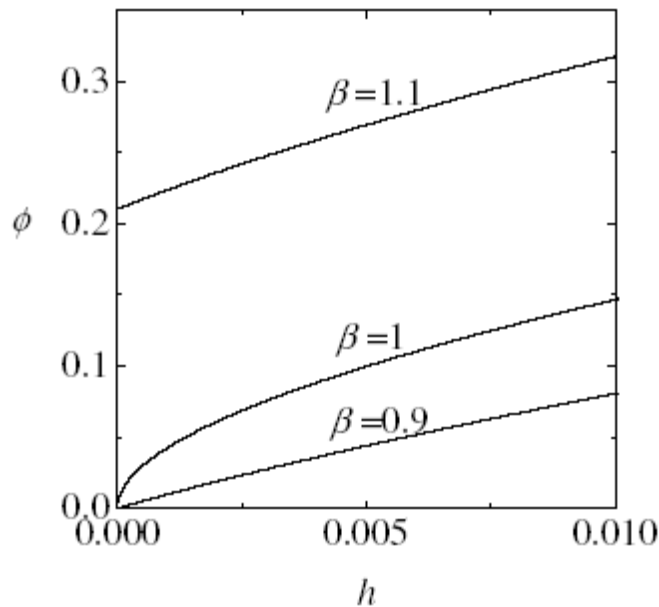


FIG. 1. Ratio of mean square velocities,  $\phi$ , as a function of the mass ratio parameter  $h$  for  $\beta = 0.9, 1$ , and  $1.1$ .

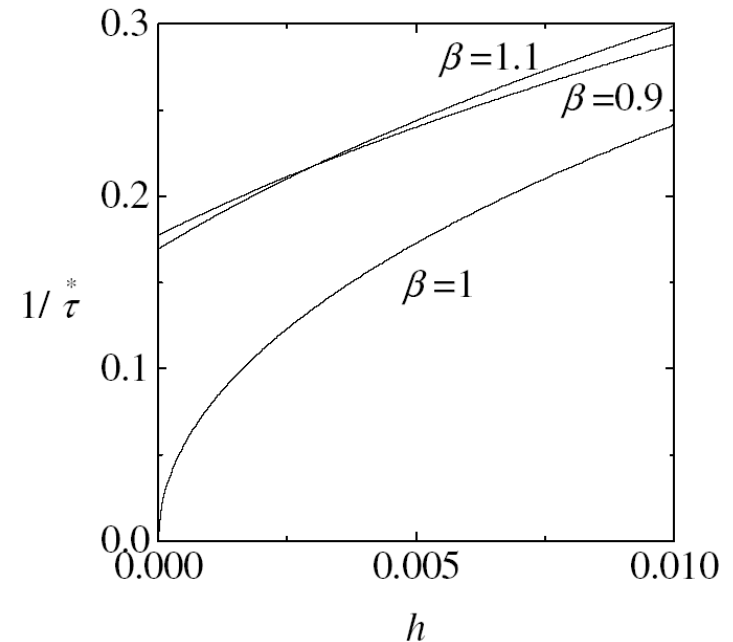


FIG. 3. Inverse characteristic time  $\tau^{*-1} \equiv (\nu^* \tau)^{-1}$  as a function of the mass ratio parameter  $h$  for  $\beta = 0.9, 1$ , and  $1.1$ .

# Case (II) $1 - a_{22} \sim h_2, x_1/h_2 \ddot{O} 0$

How good is the Maxwellian approximation?

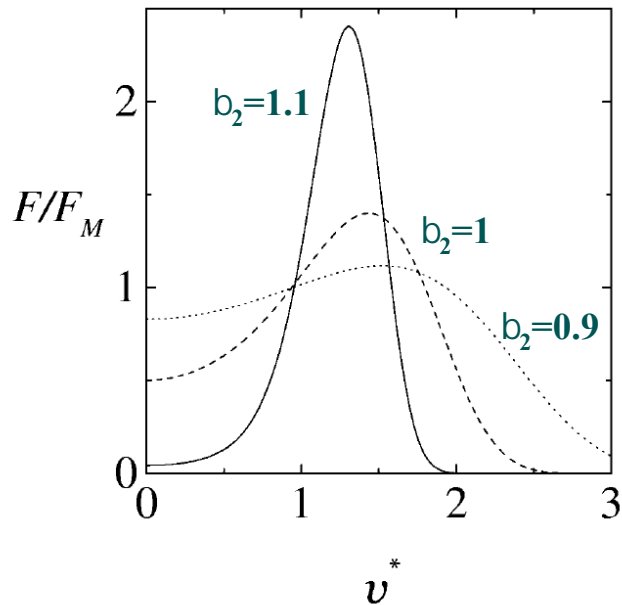


FIG. 4. Velocity distribution function of the impurity particle,  $F$ , relative to the Maxwellian,  $F_M$ , for  $h = 10^{-2}$  and  $\beta = 0.9$  (dotted line),  $\beta = 1$  (dashed line), and  $\beta = 1.1$  (solid line).

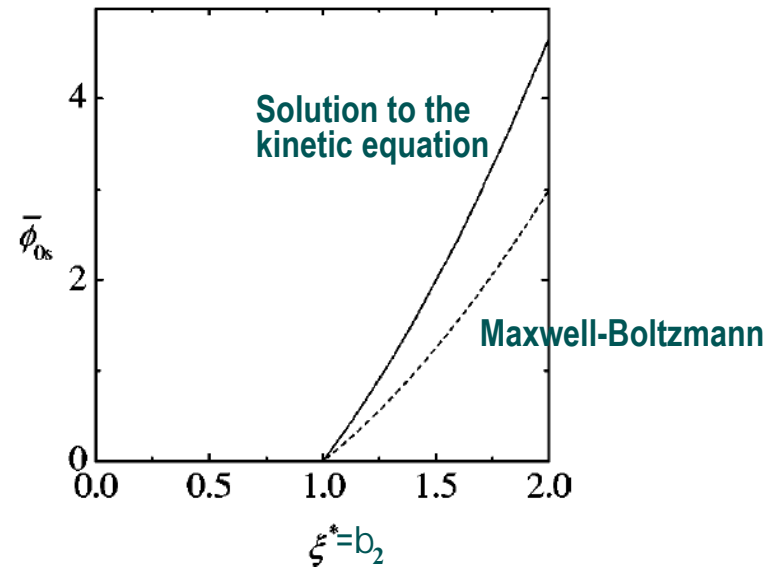


FIG. 9. Plot of the order parameter in the deterministic limit,  $\bar{\phi}_{0s}$ , as a function of  $\xi^*$ . The dashed line is the maximum entropy estimate  $\bar{\phi}_s = \xi^{*2} - 1$  of Sec. II.



# And if the system is heated?

□ Gaussian thermostat

$$\partial_t f_i(v) \rightarrow \partial_t f_i(v) + \gamma \frac{\partial}{\partial \mathbf{v}} \cdot \mathbf{v} f_i(v)$$

NESS:  $z_1 = z_2$  NO CHANGES

□ White noise

$$\partial_t f_i(v) \rightarrow \partial_t f_i(v) - D \frac{\partial^2}{\partial v^2} f_i(v)$$

NESS:  $z_1 f = z_2$  MINOR CHANGES

# Conclusions

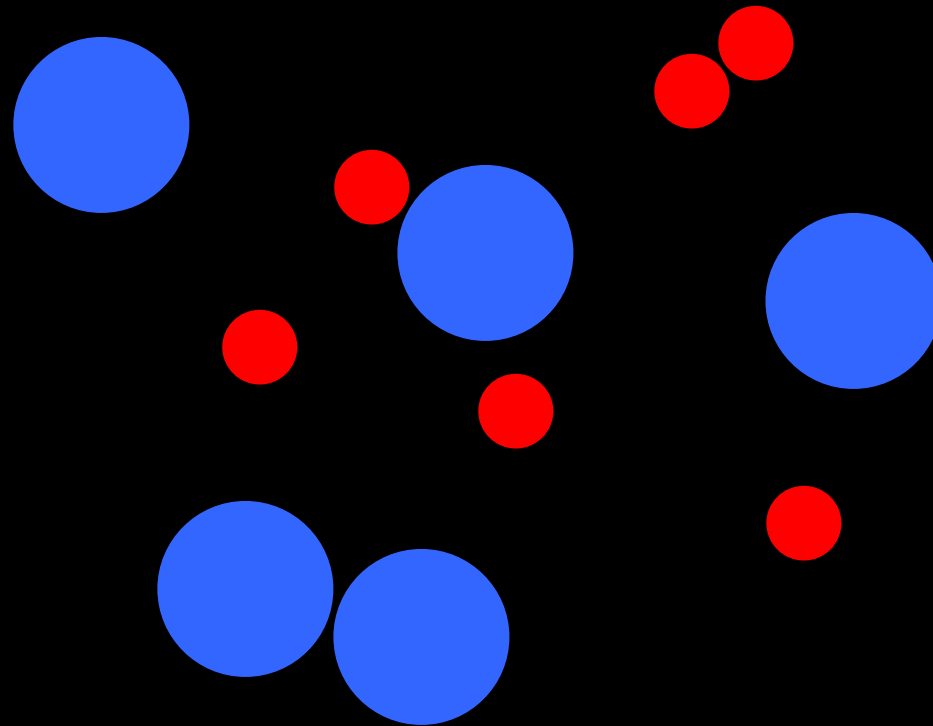
□ Depending on the control parameters (coefficients of restitution, size ratio, and concentrations), the mean square velocity ratio,  $\langle v_1^2 \rangle / \langle v_2^2 \rangle$  (and the temperature ratio  $T_1/T_2$ ) in a free cooling granular mixture exhibit a rich diversity of scaling behaviors in the disparate-mass limit  $m_1/m_2 \gg 1$ , ranging from the “sub-normal” state ( $T_1/T_2 \ll 0$ ) to the “super-ordered” state ( $\langle v_1^2 \rangle / \langle v_2^2 \rangle \gg 1$ ).

□ If the cross collisions are **inelastic** ( $a_{12} < 1$ ), the state is always “ordered” ( $\langle v_1^2 \rangle / \langle v_2^2 \rangle < 1$ ). As a consequence, in this case there is neither Brownian dynamics (when  $x_1 \ll 0$ ) nor Lorentz gas (when  $x_2 \ll 0$ ).

# Conclusions

- A “normal” state ( $T_1/T_2 \sim 1$ ) is only possible if the three types of collisions are sufficiently quasi-elastic.
- A “super-ordered” state is only possible in the Brownian limit (when  $x_1 \rightarrow 0$ ). There is no “sub-normal” state in that case.
- In the Brownian limit, there exist critical lines in the phase diagram where the state can be normal, ordered or sub-ordered.
- The same scenario as for free cooling mixtures holds essentially in the heated case.

# THANKS!



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