

Energy production rates in two-dimensional granular gases: The interplay between polydispersity, inelasticity, and roughness

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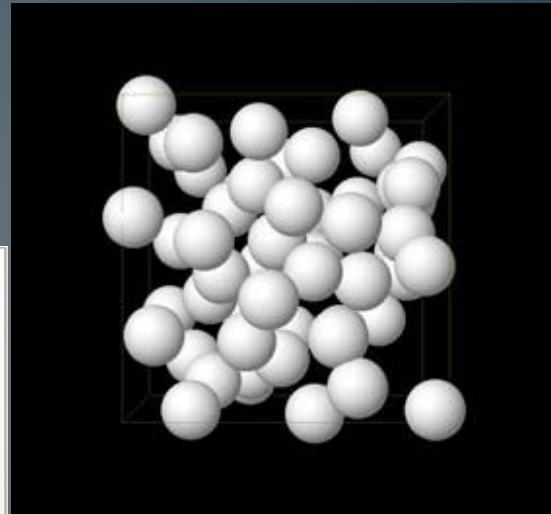
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What is a granular gas?

- It is a conglomeration of discrete solid, macroscopic particles characterized by a loss of energy whenever the grains collide.
- If the granular material is driven or shaken, such that contacts between the grains become highly infrequent, the material enters a gaseous state.

Minimal model of a granular gas: A gas of *identical smooth inelastic* hard spheres



time

coefficient of restitution 1

relative mass 1

impact parameter 1

reference frame laboratory center of mass

Elastic collision

time

coefficient of restitution 0.5

relative mass 1

impact parameter 1

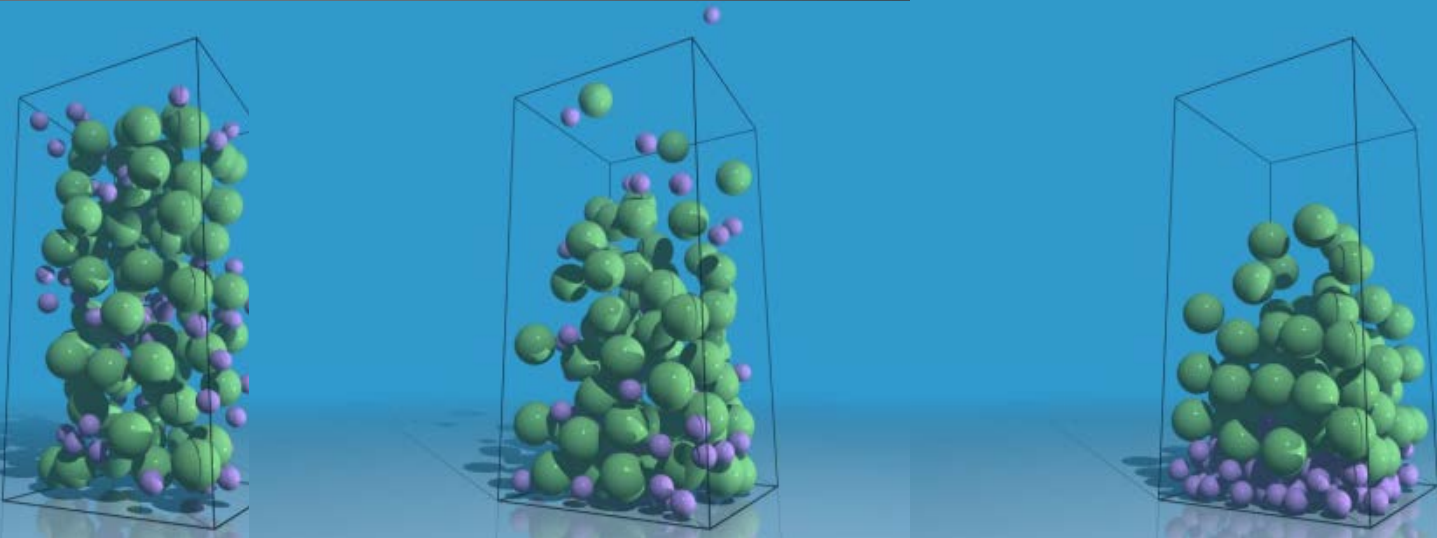
reference frame laboratory center of mass

Inelastic collision

<http://demonstrations.wolfram.com/InelasticCollisionsOfTwoSpheres/>

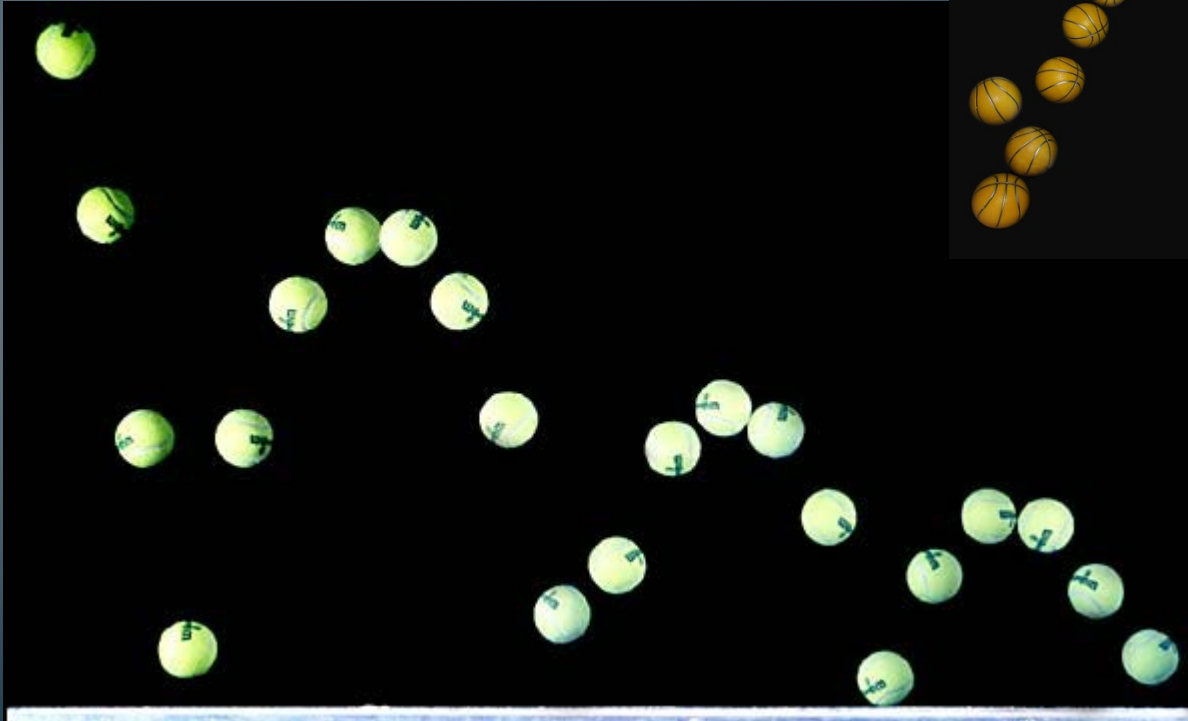
This minimal model ignores ...

Polydispersity



<http://www.cmt.york.ac.uk/~ajm143/nuts.html>

and roughness

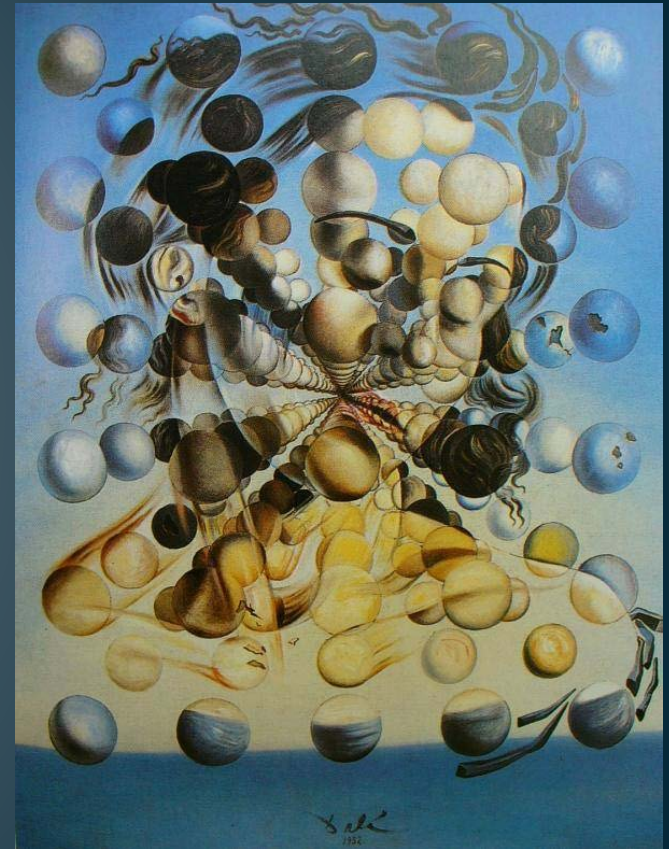


Simple model of a granular gas: A collection of *inelastic rough* hard particles

This model unveils an inherent *breakdown* of energy equipartition in granular fluids, even in homogeneous and isotropic states

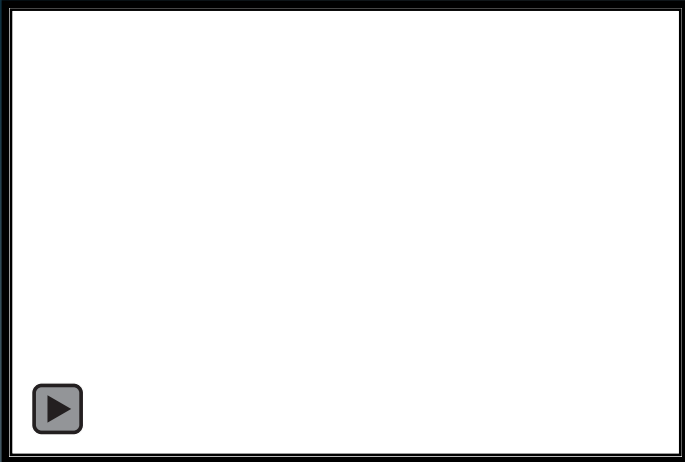


Several circles
(Kandinsky, 1926)

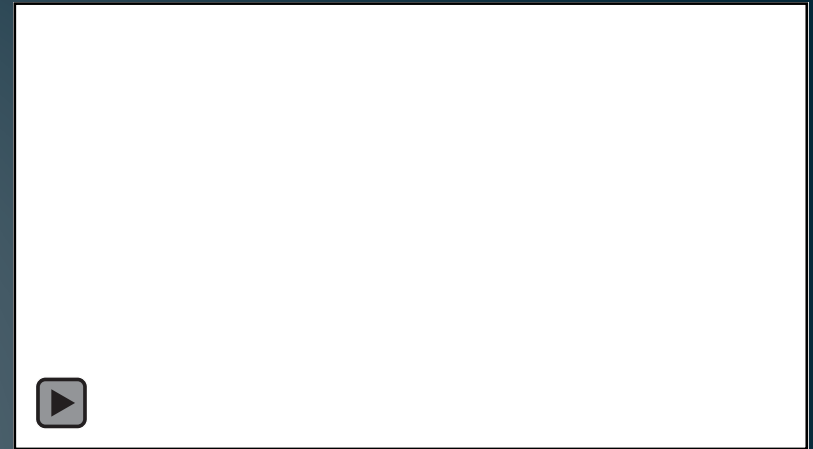


Galatea of the Spheres
(Dalí, 1952)

3Tr+3Rot

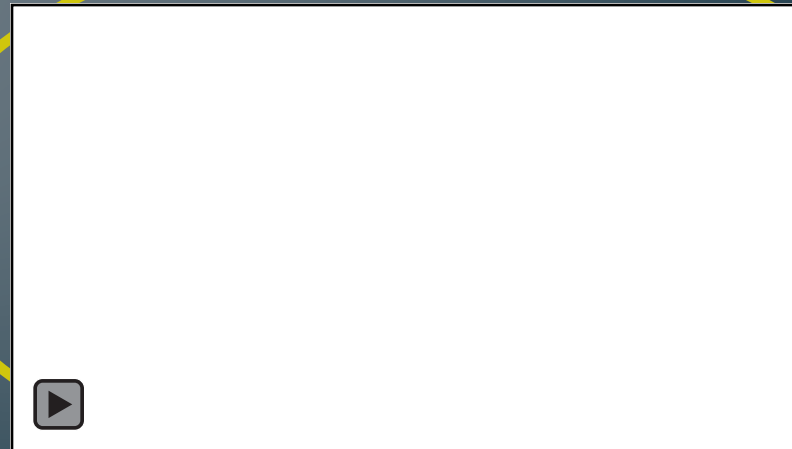


2Tr+3Rot



<https://www.shutterstock.com/video/>

2Tr+1 Rot



A motivation

PRL 118, 198003 (2017)

PHYSICAL REVIEW LETTERS

week ending
12 MAY 2017

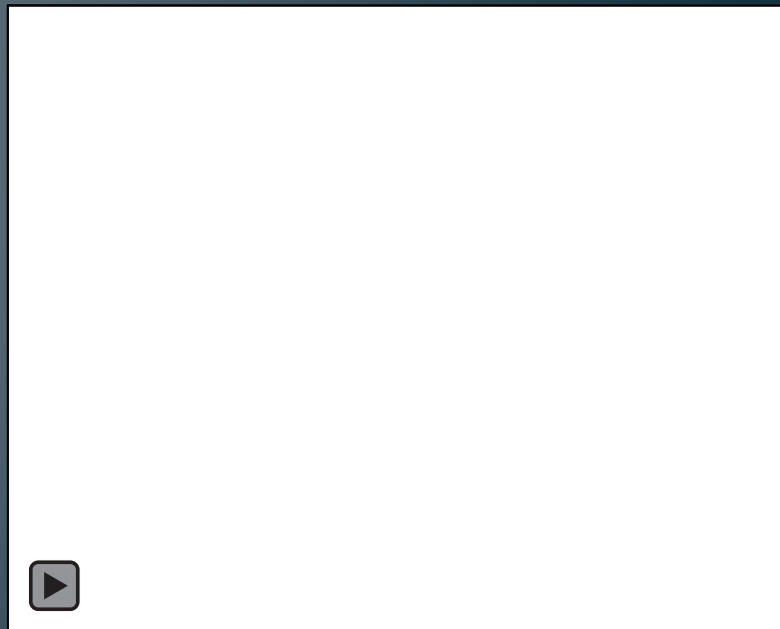


Velocity Distribution of a Homogeneously Driven Two-Dimensional Granular Gas

Christian Scholz and Thorsten Pöschel



Vibrot



Material parameters:

- Masses m_i
- Diameters σ_i
- Moments of inertia I_i
- Coefficients of normal restitution α_{ij}
- Coefficients of tangential restitution β_{ij}
- $\alpha_{ij}=1$ for perfectly elastic particles
- $\beta_{ij}=-1$ for perfectly smooth particles
- $\beta_{ij}=+1$ for perfectly rough particles

Collision rules

Cons. linear momentum:

$$m_i \mathbf{v}'_i + m_j \mathbf{v}'_j = m_i \mathbf{v}_i + m_j \mathbf{v}_j$$

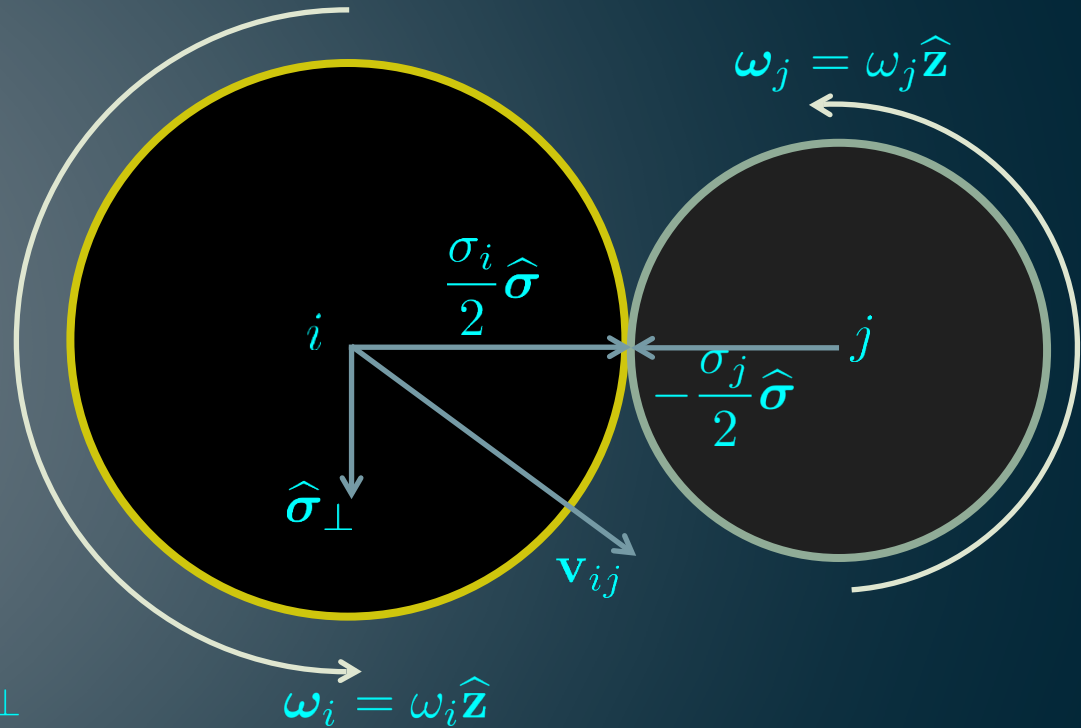
Cons. angular momentum:

$$I_i \omega'_i \pm \frac{1}{2} m_i \sigma_i (\mathbf{v}'_i \cdot \hat{\boldsymbol{\sigma}}_{\perp})$$

$$= I_i \omega_i \pm \frac{1}{2} m_i \sigma_i (\mathbf{v}_i \cdot \hat{\boldsymbol{\sigma}}_{\perp})$$

Relative velocity of the points of the spheres at contact:

$$\mathbf{w}_{ij} = \mathbf{v}_{ij} - \left(\frac{\sigma_i}{2} \omega_i + \frac{\sigma_j}{2} \omega_j \right) \hat{\boldsymbol{\sigma}}_{\perp}$$



$$\mathbf{w}'_{ij} \cdot \hat{\boldsymbol{\sigma}} = -\alpha_{ij} \mathbf{w}_{ij} \cdot \hat{\boldsymbol{\sigma}}, \quad \mathbf{w}'_{ij} \cdot \hat{\boldsymbol{\sigma}}_{\perp} = -\beta_{ij} \mathbf{w}_{ij} \cdot \hat{\boldsymbol{\sigma}}_{\perp}$$

Energy collisional loss

$$E_{ij} = \frac{1}{2}m_i v_i^2 + \frac{1}{2}m_j v_j^2 + \frac{1}{2}I_i \omega_i^2 + \frac{1}{2}I_j \omega_j^2$$

$$E'_{ij} - E_{ij} = -(1 - \alpha_{ij}^2) \times \dots \\ -(1 - \beta_{ij}^2) \times \dots$$

Energy is conserved *only* if the spheres are

- elastic ($\alpha_{ij}=1$) **and**
- **either**
 - perfectly smooth ($\beta_{ij}=-1$) **or**
 - perfectly rough ($\beta_{ij}=+1$)

Partial (granular) temperatures

Translational temperatures: $T_i^{\text{tr}} = \frac{m_i}{2} \langle (\mathbf{v}_i - \mathbf{u})^2 \rangle$

Rotational temperatures: $T_i^{\text{rot}} = I_i \langle \omega_i^2 \rangle$

Total temperature: $T = \sum_i \frac{n_i}{3n} (2T_i^{\text{tr}} + T_i^{\text{rot}})$

Collisional rates of change for temperatures

Energy production rates:

$$\xi_i^{\text{tr}} = -\frac{1}{T_i^{\text{tr}}} \left(\frac{\partial T_i^{\text{tr}}}{\partial t} \right)_{\text{coll}}, \quad \xi_i^{\text{tr}} = \sum_j \xi_{ij}^{\text{tr}} \quad \text{Binary collisions}$$

$$\xi_i^{\text{rot}} = -\frac{1}{T_i^{\text{rot}}} \left(\frac{\partial T_i^{\text{rot}}}{\partial t} \right)_{\text{coll}}, \quad \xi_i^{\text{rot}} = \sum_j \xi_{ij}^{\text{rot}}$$

Net cooling rate:

$$\zeta = -\frac{1}{T} \left(\frac{\partial T}{\partial t} \right)_{\text{coll}}, \quad \zeta = \sum_i \frac{n_i}{3nT} (2\xi_i^{\text{tr}} T_i^{\text{tr}} + \xi_i^{\text{rot}} T_i^{\text{rot}})$$

Methodology: Kinetic Theory

Ansatz on the precollisional two-body velocity distribution function:

$$f_{ij}(\mathbf{v}_i, \omega_i; \mathbf{v}_j, \omega_j) \rightarrow n_i n_j \frac{m_i m_j}{4\pi^2 T_i^{\text{tr}} T_j^{\text{tr}}} e^{-m_i \frac{(\mathbf{v}_i - \mathbf{u})^2}{2T_i^{\text{tr}}} - m_j \frac{(\mathbf{v}_j - \mathbf{u})^2}{2T_j^{\text{tr}}}} \\ \times f_i^{\text{rot}}(\omega_i) f_j^{\text{rot}}(\omega_j)$$

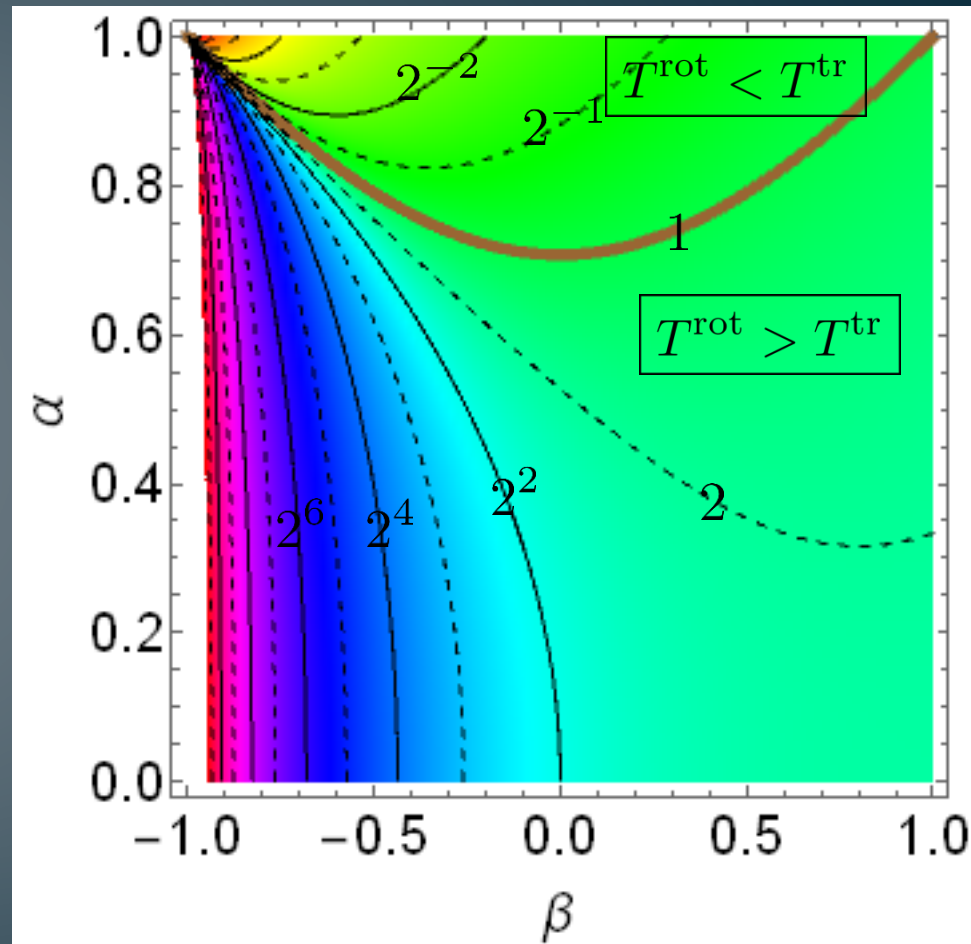
Molecular chaos+Maxwellian approx. for translational distribution

Results

$$\xi_{ij}^{\text{tr}} \ \& \ \xi_{ij}^{\text{rot}} = \text{functions of } \left\{ \begin{array}{l} m_i, m_j, I_i, I_j, \sigma_i, \sigma_j, \\ \alpha_{ij}, \beta_{ij}, \\ n_i, \quad n_j, \\ \boxed{T_i^{\text{tr}}, T_j^{\text{tr}}, T_i^{\text{rot}}, T_j^{\text{rot}}} \end{array} \right.$$

Application to the Homogeneous Cooling State. *Monodisperse system*

$$\frac{T^{\text{rot}}}{T^{\text{tr}}}$$



Application to the Homogeneous Cooling State. *Bidisperse* system

$$\alpha_{ij} = \alpha$$

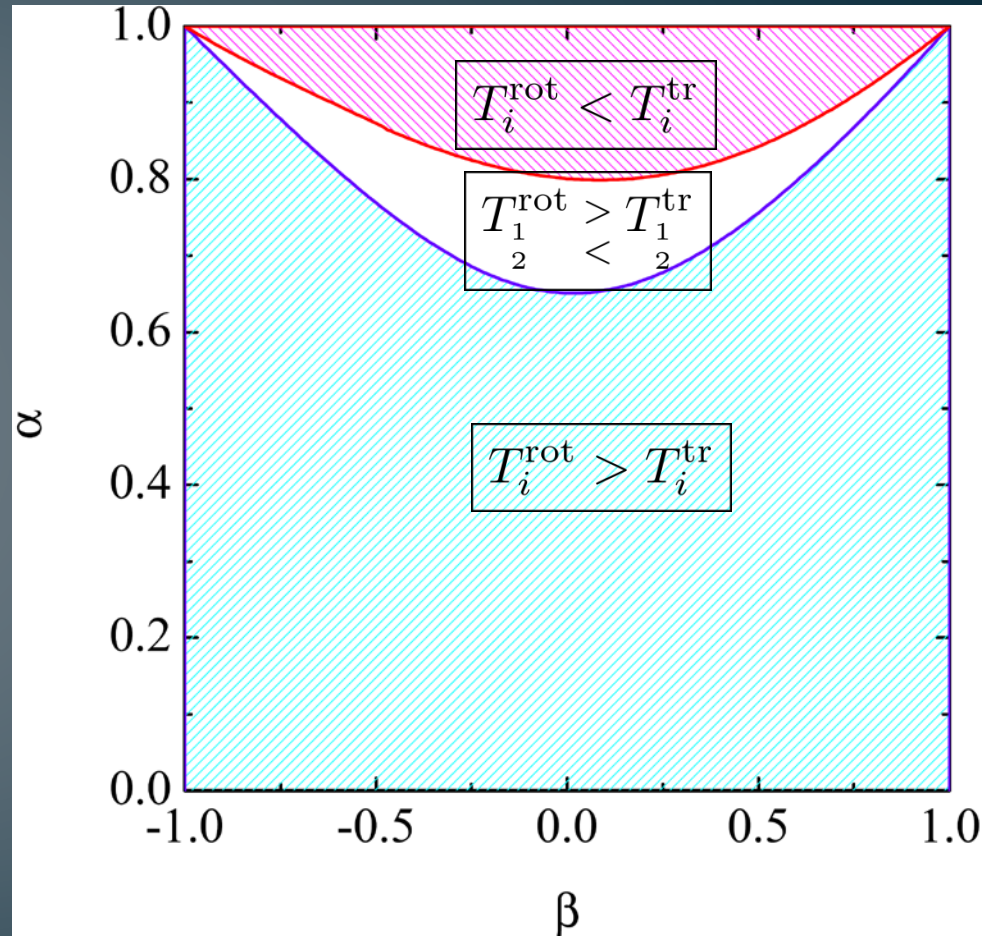
$$\beta_{ij} = \beta$$

$$\frac{n_1}{n_2} = 1$$

$$\frac{\sigma_1}{\sigma_2} = 2$$

$$\frac{m_1}{m_2} = 4$$

$$T_1^{\text{tr}} > T_2^{\text{tr}}$$



Application to the Homogeneous Cooling State. *Bidisperse system*

$$\alpha_{ij} = \alpha$$

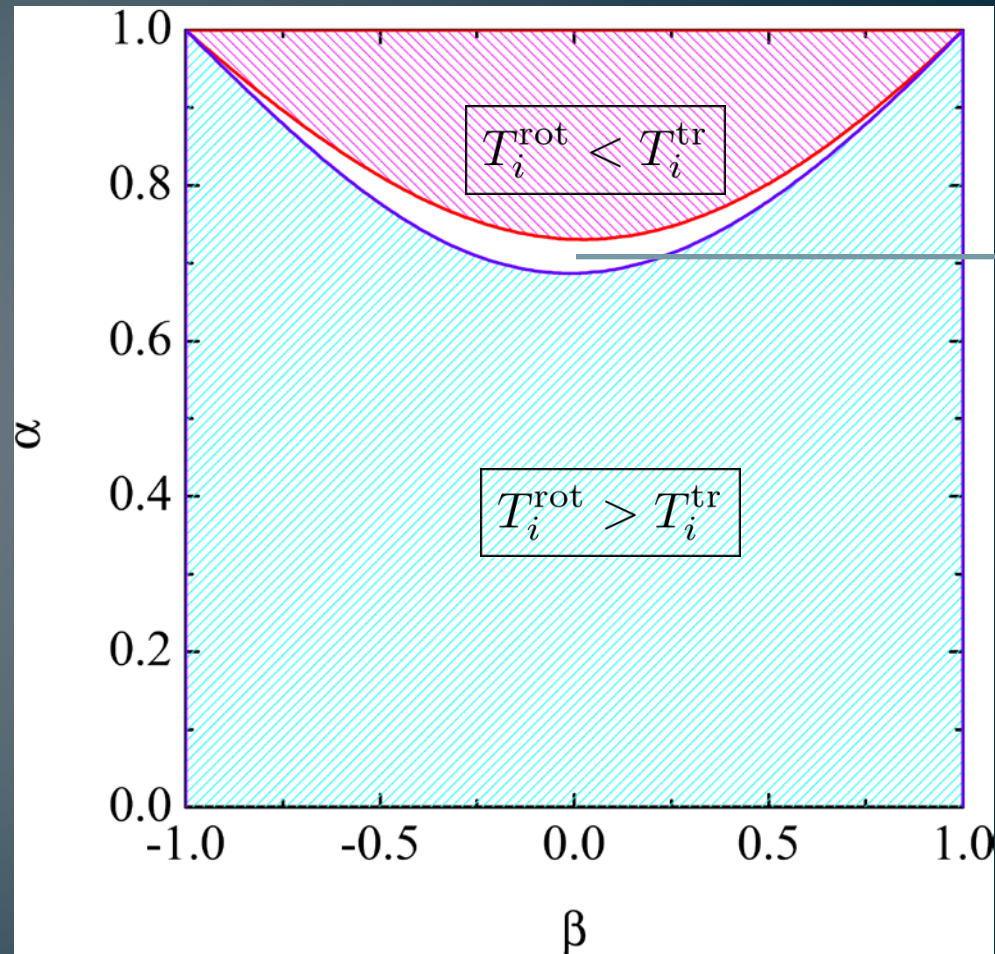
$$\beta_{ij} = \beta$$

$$\frac{n_1}{n_2} = 1$$

$$\frac{\sigma_1}{\sigma_2} = 2$$

$$\frac{m_1}{m_2} = 2$$

$$T_1^{\text{tr}} \gtrsim T_2^{\text{tr}}$$



$$\begin{matrix} T_1^{\text{rot}} > T_1^{\text{tr}} \\ T_2 < T_2 \end{matrix}$$

Application to the Homogeneous Cooling State. *Bidisperse* system

$$\alpha_{ij} = \alpha$$

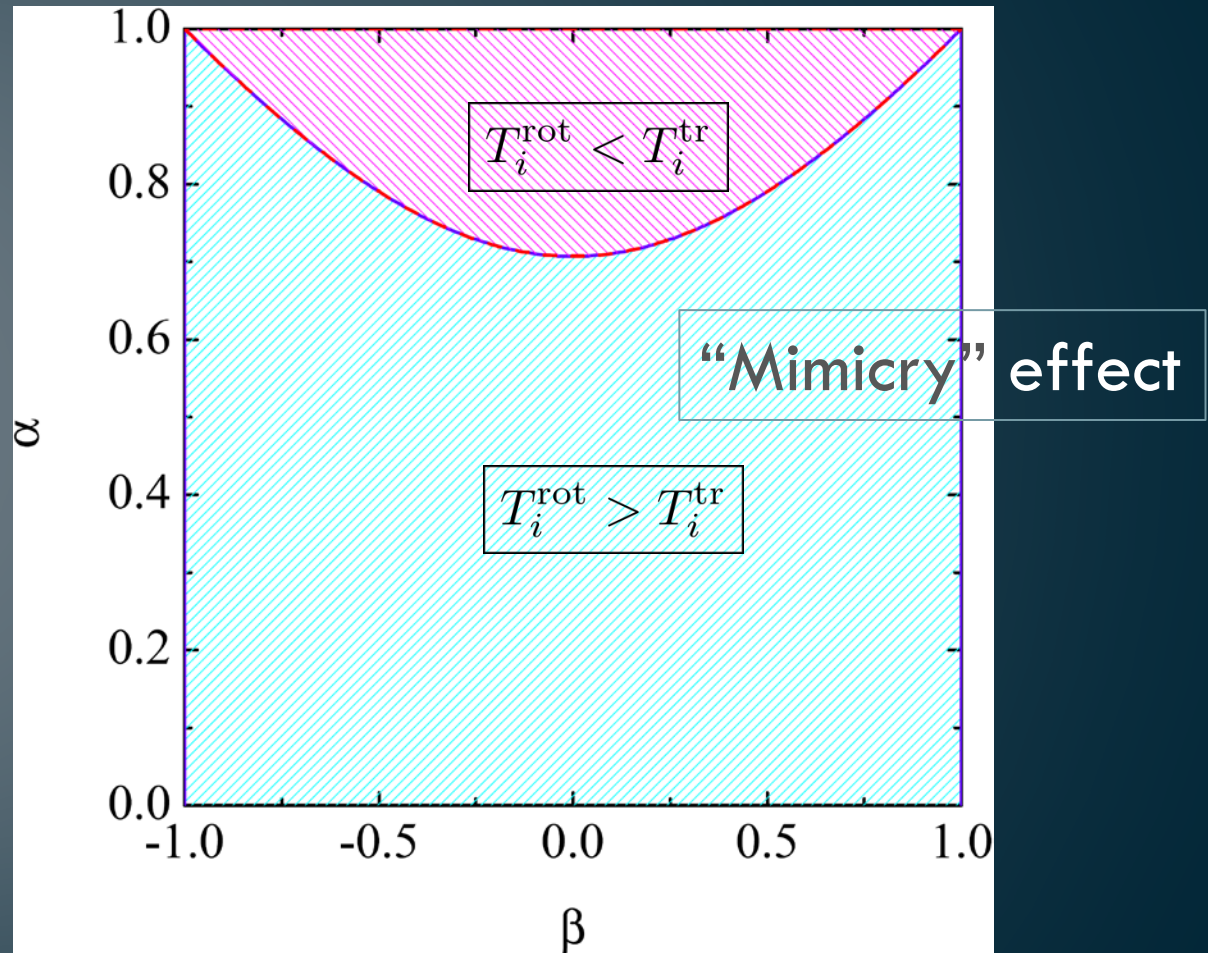
$$\beta_{ij} = \beta$$

$$\frac{n_1}{n_2} = 1$$

$$\frac{\sigma_1}{\sigma_2} = 2$$

$$\frac{m_1}{m_2} = 1.565$$

$$T_1^{\text{tr}} = T_2^{\text{tr}}$$
$$T_1^{\text{rot}} = T_2^{\text{rot}}$$



Application to the Homogeneous Cooling State. *Bidisperse system*

$$\alpha_{ij} = \alpha$$

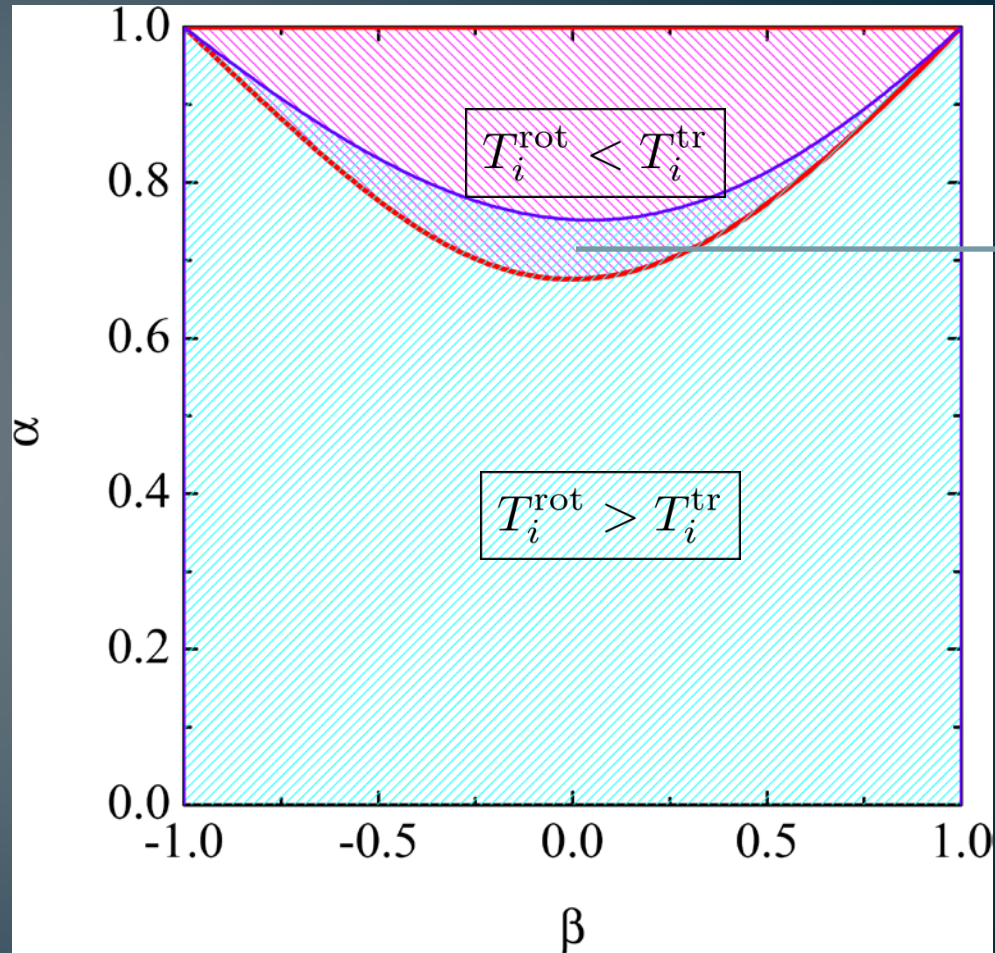
$$\beta_{ij} = \beta$$

$$\frac{n_1}{n_2} = 1$$

$$\frac{\sigma_1}{\sigma_2} = 2$$

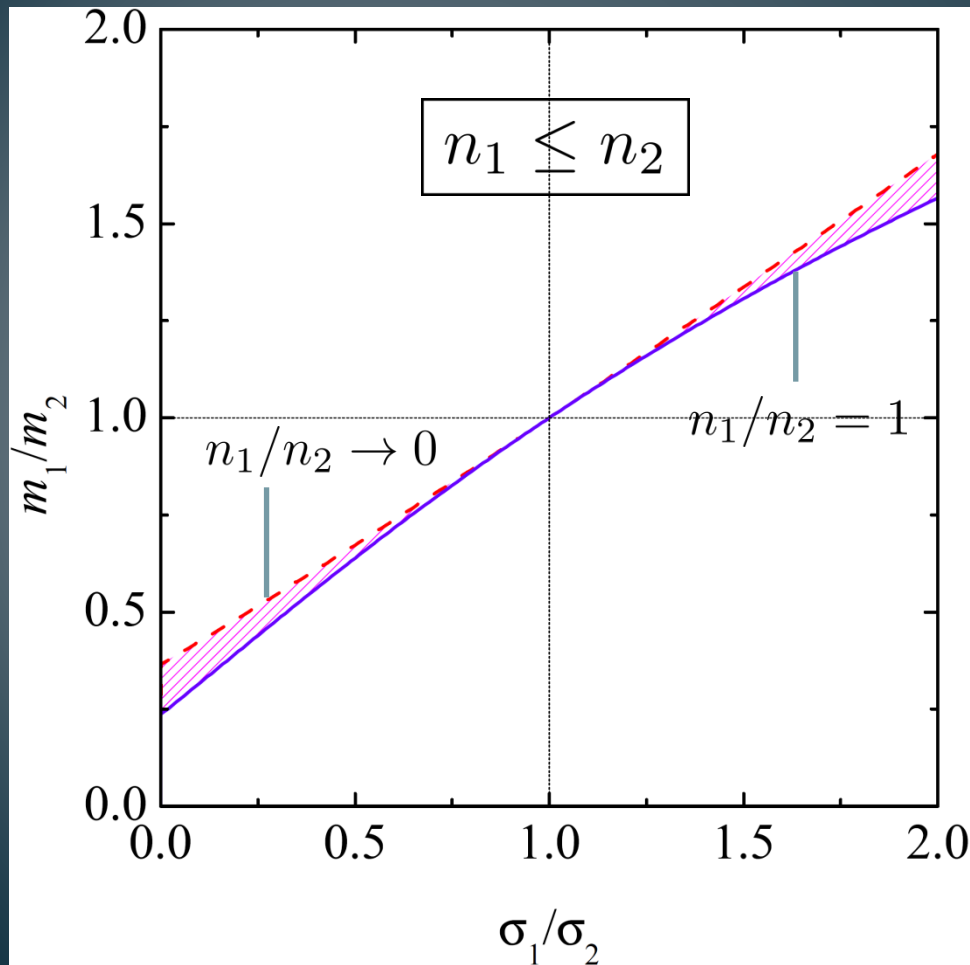
$$\frac{m_1}{m_2} = 1$$

$$T_1^{\text{tr}} < T_2^{\text{tr}}$$



$$\begin{matrix} T_1^{\text{rot}} < T_1^{\text{tr}} \\ T_2^{\text{rot}} > T_2^{\text{tr}} \end{matrix}$$

Conditions for *mimicry*



The smaller spheres must have a larger solid density than the biggest spheres

$$\frac{m_1}{m_2} \approx \frac{1}{3} \left(1 + 2 \frac{\sigma_1}{\sigma_2} \right)$$

Conclusions and outlook

- A very rich interplay between polydispersity, inelasticity, and roughness exists.
- An *intruder* component can “disguise” as the host monocomponent gas (from the point of view of mean kinetic energies): *Mimicry* effect.
- Extensions to steady states (e.g., white-noise thermostat) are straightforward.
- Comparison with computer simulations are planned.
- Next step for monocomponent gases: Derivation of the Navier-Stokes hydrodynamic equations.

THANK
YOU!

What people think about during your conference talk

