

# Hydrodynamics for granular flow at low density: Navier-Stokes and Burnett constitutive equations

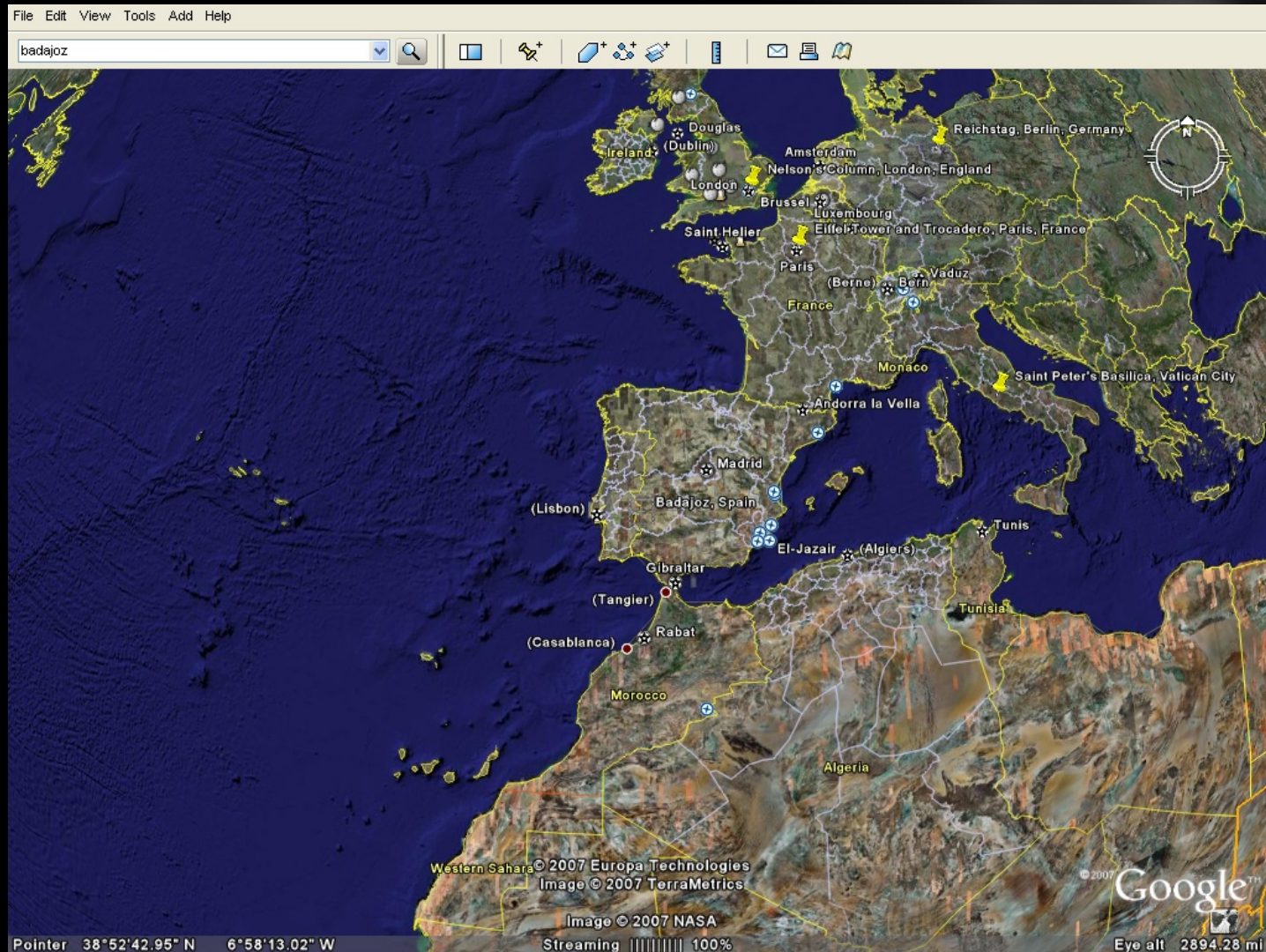


**Andrés Santos**

*Universidad de Extremadura. Badajoz, Spain*



# My Badajoz-Kyoto connection: The last 25 years



# October 1991: Fourth International Workshop on Mathematical Aspects of Fluid and Plasma Dynamics, Kyoto

## AN EXACT SOLUTION OF THE BOLTZMANN EQUATION FOR A BINARY MIXTURE

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Universidad de Extremadura  
06071 Badajoz, Spain

### ABSTRACT

The set of coupled Boltzmann equations for a binary mixture of "colored" Maxwell molecules in a steady shear flow state has been solved. Color diffusion is generated in the system by means of an external field. The velocity moments can be expressed in terms of the solution of a quartic equation. In particular, the color conductivity and the shear viscosity coefficients have been obtained as nonlinear functions of the shear rate and the field strength.

### 1. INTRODUCTION

One of the main objectives in kinetic theory is the search for exact solutions of the nonlinear Boltzmann equation. Those solutions are generally hard to find, especially due to the mathematical difficulties embodied in the Boltzmann collision term. The interest for exact solutions has been greatly stimulated by the discovery of an explicit solution for Maxwell molecules in a spatially homogeneous situation, the so-called BKW-mode.<sup>1</sup> In the case of inhomogeneous states, the most physically interesting solutions correspond to planar shear flow at uniform temperature and density (usually referred to as "uniform shear flow")<sup>2</sup> and steady heat flow at constant pressure.<sup>3</sup> Both solutions refer to Maxwell molecules and are constructed in terms of the velocity moments of the distribution function.

# November 1997: Prof. Sone visits Badajoz

From: Yoshio Sone <sone@sumi.ac.jp>  
To: "Andres Santos" <andres@ucl.ac.uk>  
Subject: RE: Some small details  
Date: Wed, 12 Nov 1997 09:44:38

Dear Professor Santos,  
Thank you very much for your advice.  
I am very happy to give a seminar at your university.  
The title is  
"Flows induced by temperature difference  
and its finite effect on the behavior of the gas"

The video of flows induced by temperature difference  
on Wednesday is convenient to me.  
Best Regards,  
Yoshio Sone



# March-April 1999: JSPS Fellow, Kyoto



# July 2008: RGD 26, Kyoto



# January 2009: Prof. Aoki visits Badajoz



**ANUNCIO DE SEMINARIO  
DEL DEPARTAMENTO DE  
FÍSICA**

**Taylor-Couette flows of a vapor-gas mixture:  
Bifurcation in the near continuum regime**

**Prof. Kazuo Aoki**  
Kyoto University

- Jueves, 29 de enero de 2009
- 12 horas
- Sala de Tesis de la Facultad de Ciencias

# July 2009: YITP long-term workshop, Kyoto





May 2016:  
Sone & Aoki's *fest*



# Hydrodynamics for granular flow at low density: Navier-Stokes and Burnett constitutive equations



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# Outline

- Introduction. Granular hydrodynamics
- The inelastic rough hard-sphere model (IRHSM). Navier-Stokes coefficients
- The inelastic Maxwell model (IMM)  
Burnett coefficients
- Conclusions

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# What is a granular material?

- It is a conglomeration of discrete solid, macroscopic particles characterized by a **loss of energy** whenever the grains collide.
- The constituents must be large enough such that they are not subject to thermal motion fluctuations. Thus, the lower size limit for grains is about  $1 \mu\text{m}$ .



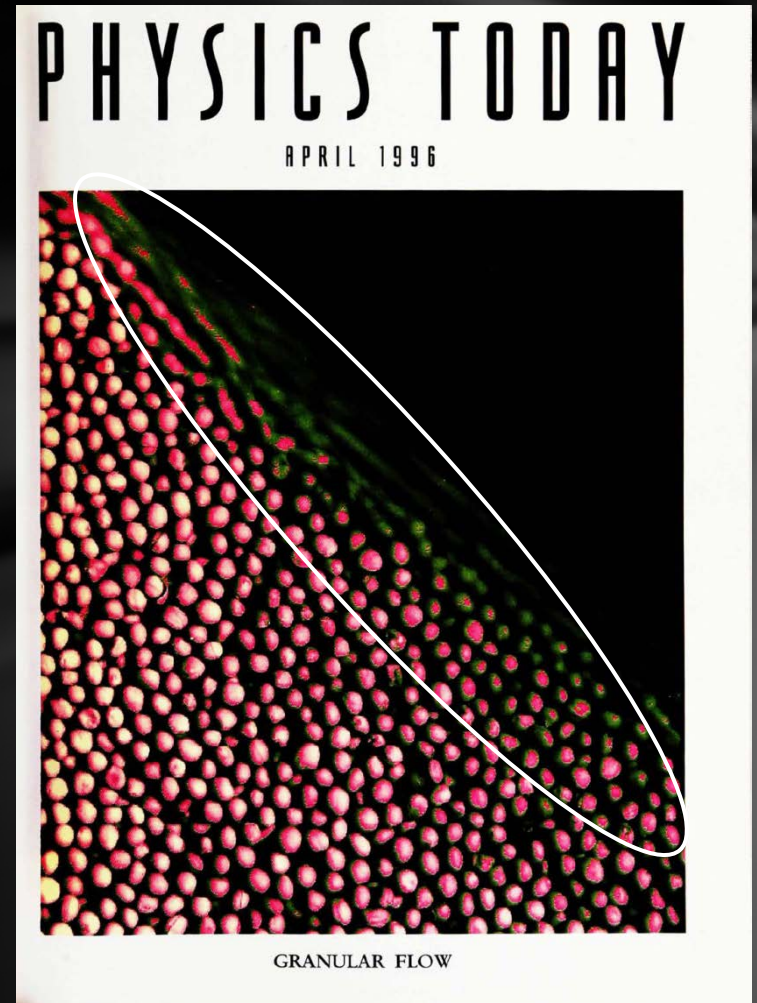
# What is a granular *fluid*?

When the granular matter is driven and energy is fed into the system (e.g., by shaking) such that the grains are not in constant contact with each other, the granular material is said to *fluidize*.

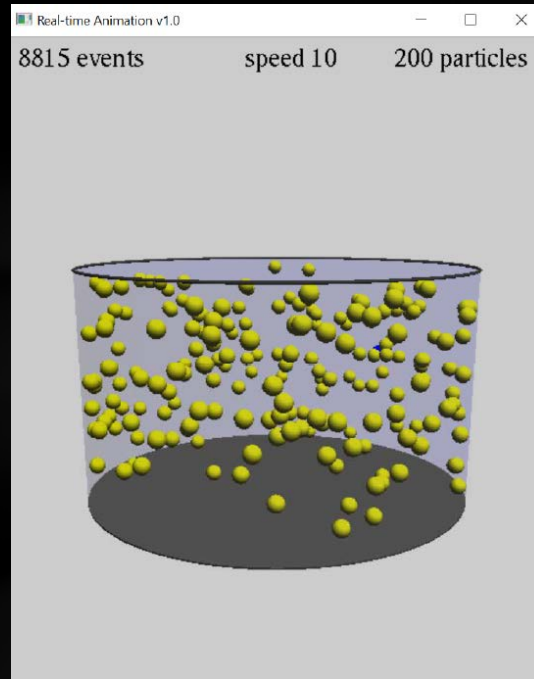
**Granular gas**: Mean free path much larger than the grain size



KINETIC THEORY



# Granular gas: Dissipative collisions

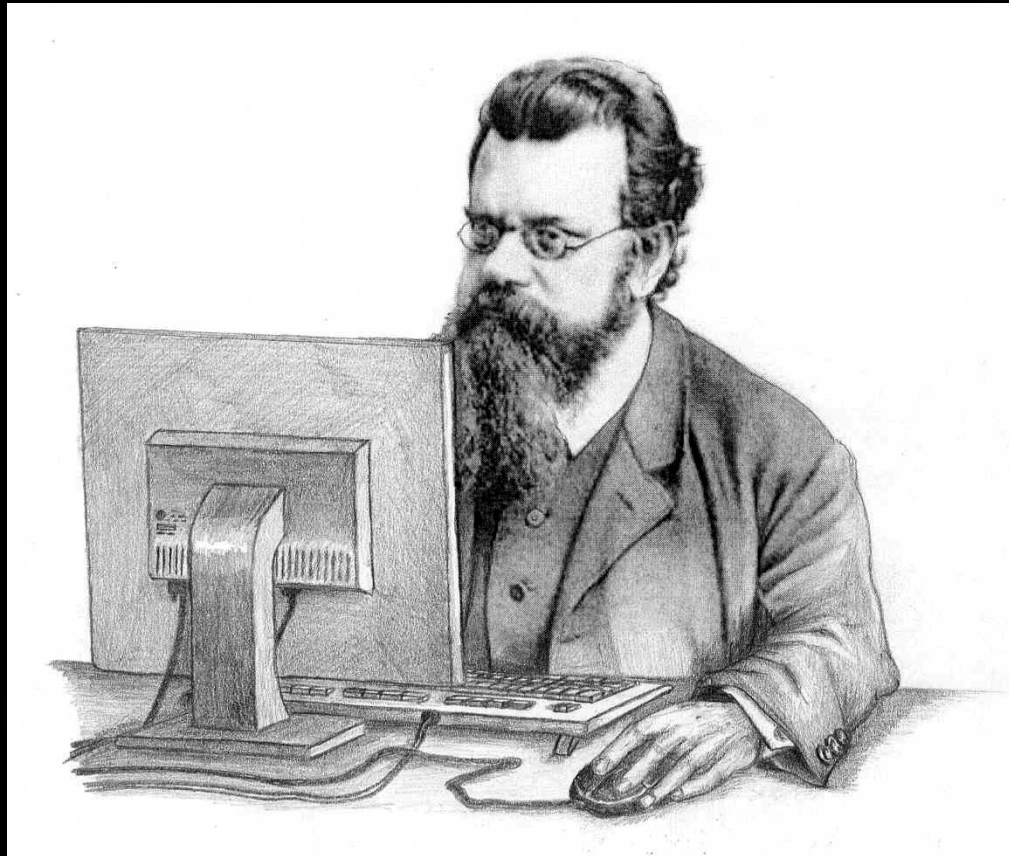


Demo by Sergei Mechov

# KINETIC THEORY



(Cartoon by Bernhard Reischl, University of Vienna)



**Boltzmann equation:**

$$\partial_t f(\mathbf{r}, \mathbf{v}, t) + \mathbf{v} \cdot \nabla f(\mathbf{r}, \mathbf{v}, t) = J[\mathbf{r}, \mathbf{v}, t|f]$$

Dissipative collisions

# HYDRODYNAMICS

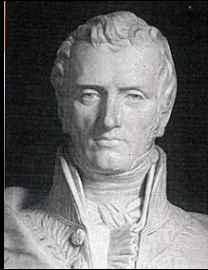
# Hydrodynamic balance equations

$$\left. \begin{aligned}
 \text{Mass conservation:} & \quad \mathcal{D}_t n + n \nabla \cdot \mathbf{u} = 0 \\
 \text{Momentum conservation:} & \quad \rho \mathcal{D}_t \mathbf{u} + \nabla \cdot \mathbf{P} = 0 \\
 \text{Energy } \textit{dissipation}: & \quad \mathcal{D}_t T + \frac{2}{nd} (\nabla \cdot \mathbf{q} + \mathbf{P} : \nabla \mathbf{u}) = -\zeta T
 \end{aligned} \right\}$$

Dimensionality
Cooling rate

$$(\mathcal{D}_t \equiv \partial_t + \mathbf{u} \cdot \nabla)$$

# Navier-Stokes (NS) constitutive equations



Claude-Louis Navier  
(1785-1836)



George Gabriel Stokes  
(1819-1903)



Jean-Baptiste Joseph Fourier  
(1768-1830)

$$P_{ij} = p\delta_{ij} - \eta \left( \nabla_i u_j + \nabla_j u_i - \frac{2}{d} \delta_{ij} \nabla \cdot \mathbf{u} \right) - \eta_b \delta_{ij} \nabla \cdot \mathbf{u}$$

Shear viscosity
Bulk viscosity

$$\mathbf{q} = -\lambda \nabla T - \mu \nabla n$$

Dufour-like coefficient
Thermal conductivity

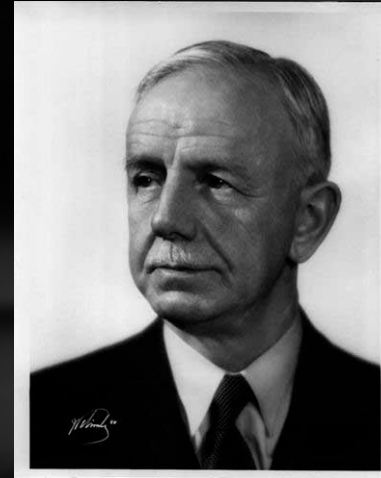
$$\zeta = \zeta^{(0)} - \xi \nabla \cdot \mathbf{u}$$

Cooling rate transport coefficient

# Methodology: Chapman-Enskog method



Sydney Chapman  
(1888-1970)



David Enskog  
(1884-1947)

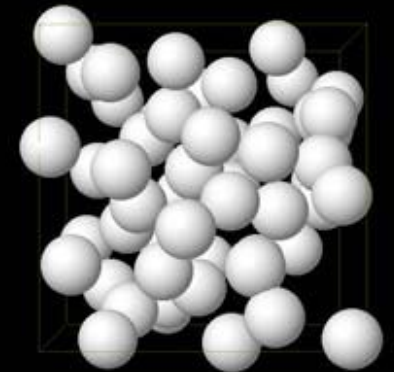
$$f = f^{(0)} + \epsilon f^{(1)} + \epsilon^2 f^{(2)} + \dots, \quad \epsilon \sim \nabla$$

Navier-  
Stokes

Burnett

# MODELS OF GRAINS

Standard model of a granular gas:  
A gas of identical *inelastic smooth* hard spheres  
(ISHSM)



Constant coefficient of *normal* restitution  $\alpha$

time  
coefficient of restitution 1  
relative mass 1  
impact parameter 1  
reference frame laboratory center of mass

Elastic collision

time  
coefficient of restitution 0.5  
relative mass 1  
impact parameter 1  
reference frame laboratory center of mass

Inelastic collision

<http://demonstrations.wolfram.com/InelasticCollisionsOfTwoSpheres/>

## Hydrodynamics for granular flow at low density

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(Received 13 March 1998; revised manuscript received 8 June 1998)

The hydrodynamic equations for a gas of hard spheres with dissipative dynamics are derived from the Boltzmann equation. The heat and momentum fluxes are calculated to Navier-Stokes order and the transport coefficients are determined as explicit functions of the coefficient of restitution. The dispersion relations for the corresponding linearized equations are obtained and the stability of this linear description is discussed. This requires consideration of the linear Burnett contributions to the energy balance equation from the energy sink term. Finally, it is shown how these results can be imbedded in simpler kinetic model equations with the potential for analysis of more complex states.



Hydrodynamic  
order ↑

Burnett	2014 ( $dD$ , Exact)	?	?
Navier-Stokes (NS)	2003 ( $dD$ , Exact)	1998 (Sonine appr.)	2014 (3D, Sonine appr.)
	Inelastic Maxwell model (IMM)	Inelastic smooth hard-sphere model (ISHSM)	Inelastic rough hard-sphere model (IRHSM)

→ Model complexity

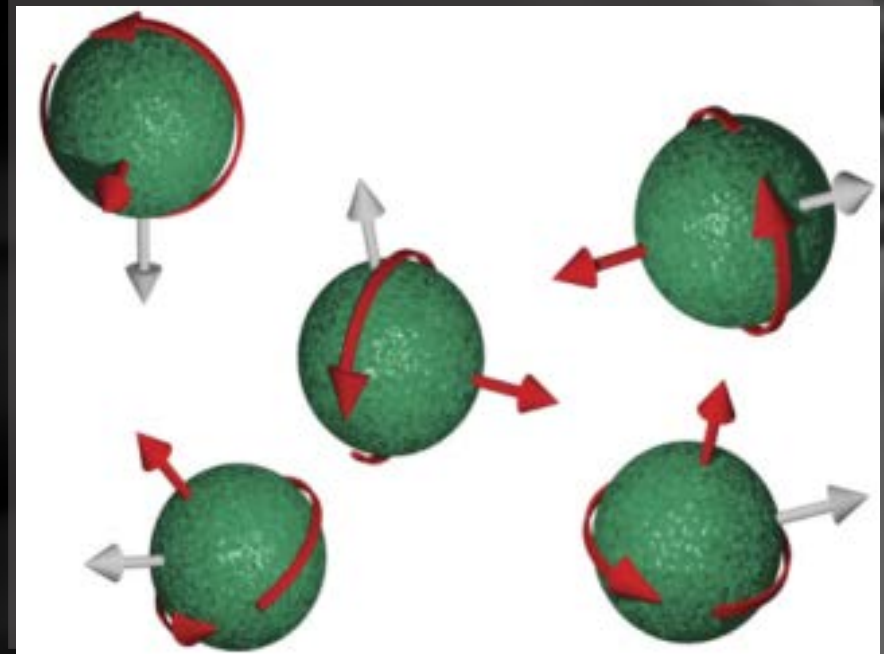
# Outline

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# Inelastic rough hard-sphere model (IRHSM)

## Material parameters:

- Mass  $m$
- Diameter  $\sigma$
- Moment of inertia  $I$  ( $\kappa=4I/m\sigma^2$ )
- Coefficient of normal restitution  $\alpha$
- Coefficient of tangential restitution  $\beta$
- $\alpha=1$  for perfectly elastic particles
- $\beta=-1$  for perfectly smooth particles
- $\beta=+1$  for perfectly rough particles



This model unveils the inherent breakdown of equilibrium and energy equipartition in granular fluids, even in *homogeneous* and isotropic states

# Collision rules

Cons. linear momentum:

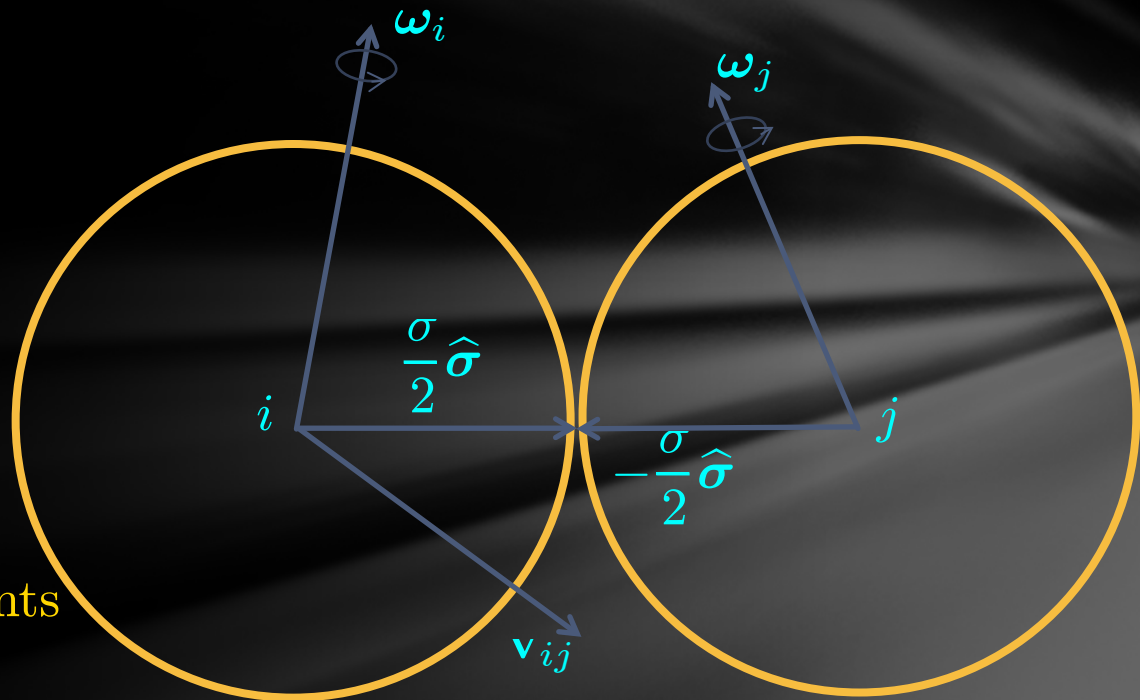
$$\mathbf{v}'_i + \mathbf{v}'_j = \mathbf{v}_i + \mathbf{v}_j$$

Cons. angular momentum:

$$\begin{aligned} I\boldsymbol{\omega}'_{i,j} &\mp m \frac{\sigma_i}{2} \hat{\boldsymbol{\sigma}} \times \mathbf{v}'_{i,j} \\ &= I\boldsymbol{\omega}_{i,j} \mp m \frac{\sigma_i}{2} \hat{\boldsymbol{\sigma}} \times \mathbf{v}_{i,j} \end{aligned}$$

Relative velocity of the points  
of the spheres at contact:

$$\bar{\mathbf{v}}_{ij} = \mathbf{v}_{ij} - \frac{\sigma}{2} \hat{\boldsymbol{\sigma}} \times (\boldsymbol{\omega}_i + \boldsymbol{\omega}_j)$$



$$\left| \hat{\boldsymbol{\sigma}} \cdot \bar{\mathbf{v}}'_{ij} = -\alpha \hat{\boldsymbol{\sigma}} \cdot \bar{\mathbf{v}}_{ij}, \quad \hat{\boldsymbol{\sigma}} \times \bar{\mathbf{v}}'_{ij} = -\beta \hat{\boldsymbol{\sigma}} \times \bar{\mathbf{v}}_{ij} \right|$$

# Energy collisional loss

$$E_{ij} = \frac{1}{2}mv_i^2 + \frac{1}{2}mv_j^2 + \frac{1}{2}I\omega_i^2 + \frac{1}{2}I\omega_j^2$$


$$E'_{ij} - E_{ij} = -(1 - \alpha^2) \times \dots \\ -(1 - \beta^2) \times \dots$$

Energy is conserved *only* if the spheres are

- elastic ( $\alpha=1$ ) **and**
- **either**
  - perfectly smooth ( $\beta=-1$ ) **or**
  - perfectly rough ( $\beta=+1$ )

coefficient of normal restitution   $\alpha = 1$   
 coefficient of tangential restitution   $\beta = -1$   
 relative mass   
 impact parameter   
 initial angular velocity of the left particle   
 time   
 reference frame


energy loss (lab frame) = 0%



Elastic & smooth

coefficient of normal restitution   $\alpha = 1$   
 coefficient of tangential restitution   $\beta = 1$   
 relative mass   
 impact parameter   
 initial angular velocity of the left particle   
 time   
 reference frame


energy loss (lab frame) = 0%



Elastic & (perfectly) rough

coefficient of normal restitution   $\alpha = 0.5$   
 coefficient of tangential restitution   $\beta = -1$   
 relative mass   
 impact parameter   
 initial angular velocity of the left particle   
 time   
 reference frame


energy loss (lab frame) = 27%



Inelastic & smooth

coefficient of normal restitution   $\alpha = 0.5$   
 coefficient of tangential restitution   $\beta = 1$   
 relative mass   
 impact parameter   
 initial angular velocity of the left particle   
 time   
 reference frame

energy loss (lab frame) = 27%



Inelastic & (perfectly) rough

<http://demonstrations.wolfram.com/InelasticCollisionsOfTwoRoughSpheres/>

# Explicit expressions

$$\tilde{\alpha} = \frac{1+\alpha}{2}, \quad \tilde{\beta} = \frac{1+\beta}{2} \frac{\kappa}{\kappa+1}$$

$$\tau_t^{(0)}/T = \tau_t = \frac{2}{1+\theta}, \quad \tau_r^{(0)}/T = \tau_r = \frac{2\theta}{1+\theta}$$

$$\theta = \sqrt{1+h^2} + h, \quad h \equiv \frac{(1+\kappa)^2}{2\kappa(1+\beta)^2} \left[ \frac{1+\beta-\kappa}{2} \alpha^2 - (1-\beta^2) \frac{1-\kappa}{1+\kappa} \right]$$

$$\nu_H \zeta^* = \frac{16}{5} \frac{\nu^2}{\nu} \frac{T}{m} \quad \theta = \sqrt{1+h^2} + h, \quad h \equiv \frac{(1+\kappa)^2}{2\kappa(1+\beta)^2} \left[ 1 - \alpha^2 - (1-\beta^2) \frac{1-\kappa}{1+\kappa} \right]$$

$$\zeta^{(0)}/\nu = \zeta^* = \frac{5}{12} \frac{1}{1+\theta} \left[ 1 - \frac{\nu}{\zeta^{(0)}} \frac{16}{5} \frac{\nu^2}{\nu} \frac{T}{m} \left( \frac{1}{1+\theta} \right) \left[ \beta^2 \frac{\theta+\kappa}{1-\alpha^2} + (1-\beta^2) \frac{\theta+\kappa}{1+\kappa} \right] \right]$$

$$\eta = (n\tau_t T/\nu) / (\nu_\eta^* - \frac{1}{2}\zeta^*) = (n\tau_t T/\nu) / (\nu_\eta^* - \frac{1}{2}\zeta^*)$$

$$\eta_b = (n\tau_t \tau_r T/\nu) \gamma_E$$

**NS coefficients**

$$\lambda = \tau_t \lambda_t + \tau_r \lambda_r, \quad \lambda_t = \frac{5}{2} \left( \frac{\tau_t^2 T^2}{m\nu} \right) \gamma_{A_t}, \quad \lambda_r = \frac{3}{2} \left( \frac{\tau_r^2 T^2}{m\nu} \right) \gamma_{A_r}$$

$$\mu = \mu_t + \mu_r, \quad \mu_t = \frac{5}{2} \left( \tau_t^2 T^2 / m\nu \right) \gamma_{B_t}, \quad \mu_r = \frac{3}{2} \left( \tau_r^2 T^2 / m\nu \right) \gamma_{B_r}$$

$$\xi = \frac{1}{2} (\tau_t \xi_t + \tau_r \xi_r) = \gamma_E \Xi_t, \quad \xi_t = \frac{5}{8} \tau_t \left[ 1 - \alpha^2 + (1 - \beta^2) \frac{1+\beta}{1+\kappa} \right] \gamma_{E_t}, \quad \xi_r = \frac{3}{8} \tau_r \left[ 1 - \alpha^2 + (1 - \beta^2) \frac{1+\beta}{1+\kappa} \right] \gamma_{E_r}$$

**Auxiliary quantities**

$$\nu_\eta^* = (\tilde{\alpha} + \tilde{\beta})(2 - \tilde{\alpha} - \tilde{\beta}) \pm \frac{\beta^2 \theta}{6\kappa} + (1 - \beta^2) \left( 1 + \frac{1}{3} \frac{\theta - 5}{1 + \kappa} \right)$$

$$\gamma_E = \frac{2}{3} (\Xi_t - \Xi_r - \zeta^*)^{-1} \gamma_{A_t} = \frac{Z_r - Z_t - 2\zeta^*}{(Y_t - 2\zeta^*)(Z_r - 2\zeta^*) - Y_r Z_t}$$

$$\Xi_t = \frac{5}{8} \tau_r \left[ 1 - \alpha^2 + (1 - \beta^2) \frac{1+\beta}{1+\kappa} \right] \gamma_{E_t} = \frac{\gamma_{A_t} (Z_r - \frac{3}{2}\zeta^*) - \gamma_{A_r} Z_t}{1 + \kappa_{A_r} (Y_t - \frac{3}{2}\zeta^*) - \gamma_{A_t} Y_r} \left( \frac{1+\beta}{1+\kappa} \right)^2$$


$$\Xi_r = \frac{5}{8} \tau_t \frac{1+\beta}{1+\kappa} \left[ \frac{\theta-2}{3} (1 - \beta^2) \frac{1+\beta}{1+\kappa} + \frac{41}{12} \frac{\kappa}{3} \left( \frac{\theta-5}{1+\kappa} \right) - \frac{4}{3} \tilde{\alpha} \tilde{\beta} - \frac{7\theta}{12} \frac{\tilde{\beta}^2}{\kappa} \right]$$


$$\Xi = \frac{5}{16} \tau_t \tau_r \left[ 1 - \alpha^2 + (1 - \beta^2) \frac{1+\beta}{1+\kappa} \right] \gamma_E = \frac{Z_t}{Y_r} \left( \frac{1+\beta}{1+\kappa} \right) \left[ \left( 1 - \frac{1}{3} \frac{\theta-5}{1+\kappa} \right) \right]$$

$$\gamma_{A_t} = \frac{Z_r - Z_t - 2\zeta^*}{(Y_t - 2\zeta^*)(Z_r - 2\zeta^*) - Y_r Z_t}, \quad Z_r = \frac{5}{6} (\tilde{\alpha} + \tilde{\beta}) + \frac{5}{18} \frac{\tilde{\beta}}{\kappa} \left( 7 - 3 \frac{\tilde{\beta}}{\kappa} - 6\tilde{\beta} - 4\tilde{\alpha} \right)$$

# Special limiting cases

Quantity	Pure smooth $(\beta = -1)$	Quasi-smooth limit $(\beta \rightarrow -1)$	Perfectly rough and elastic $(\alpha = \beta = 1)$
$\eta^*$	$\frac{24}{(1 + \alpha)(13 - \alpha)}$	$\frac{24}{(1 + \alpha)(19 - 7\alpha)}$	$\frac{6(1 + \kappa)^2}{6 + 13\kappa}$
$\eta_b^*$	0	$\frac{8}{5(1 - \alpha^2)}$	$\frac{(1 + \kappa)^2}{10\kappa}$
$\lambda^*$	$\frac{64}{(1 + \alpha)(9 + 7\alpha)}$	$\frac{48}{25(1 + \alpha)}$	$\frac{12(1 + \kappa)^2 (37 + 151\kappa + 50\kappa^2)}{25 (12 + 75\kappa + 101\kappa^2 + 102\kappa^3)}$
$\mu^*$	$\frac{1280(1 - \alpha)}{(1 + \alpha)(9 + 7\alpha)(19 - 3\alpha)}$	0	0
$\xi$	0	0	0

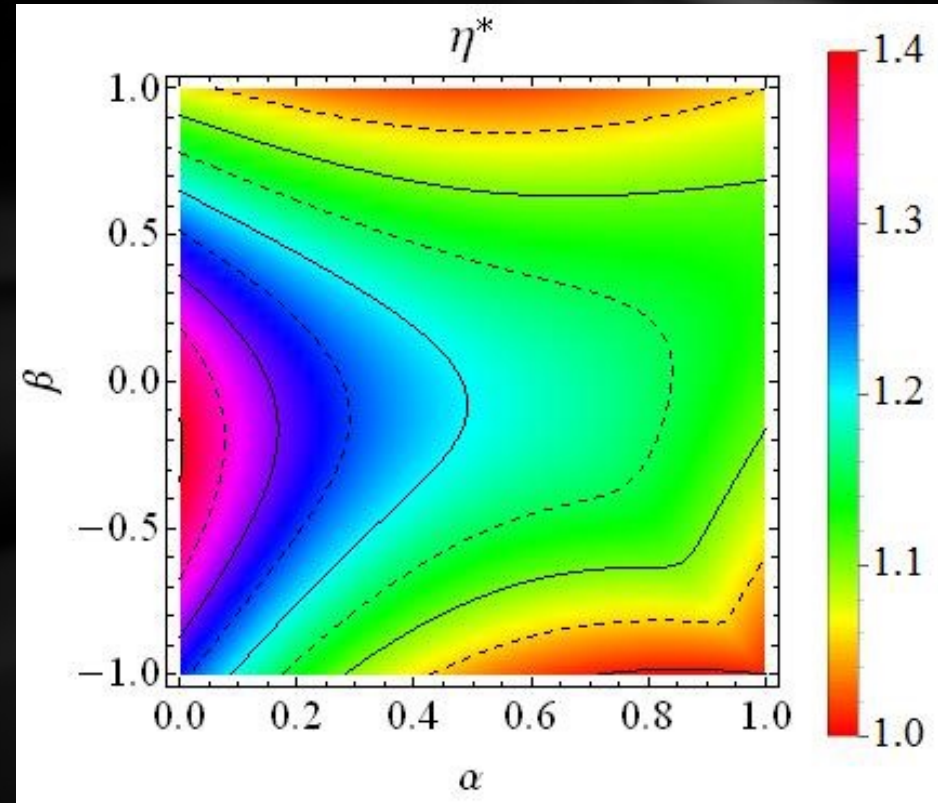
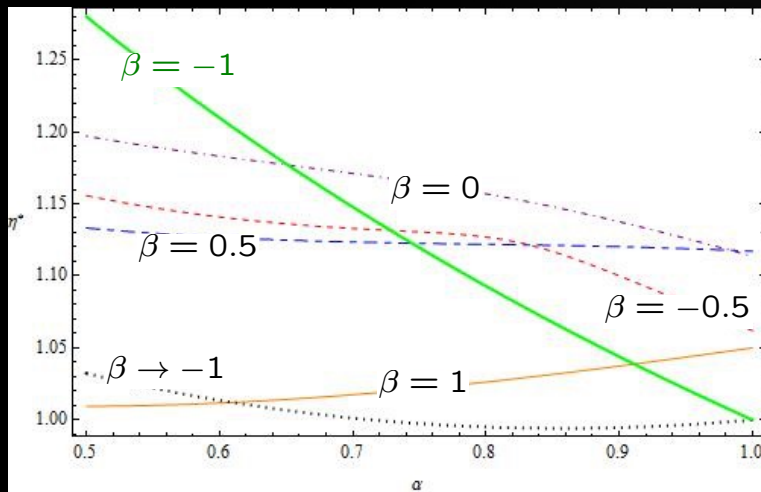
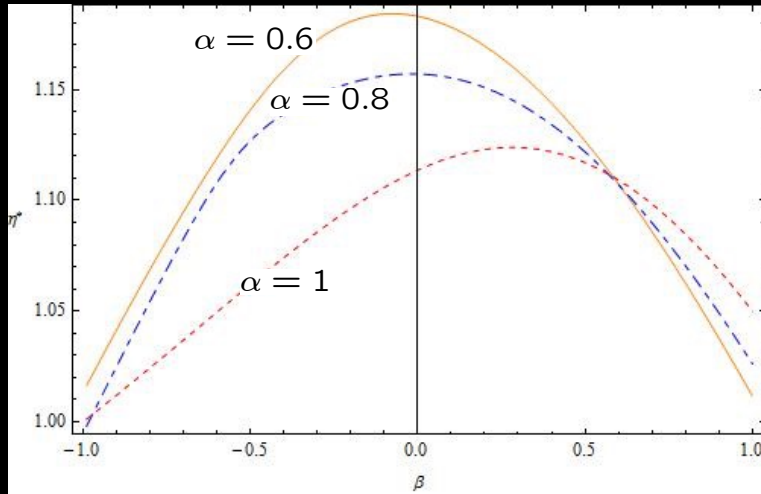
  
 Brey, Dufty, Kim, Santos  
 (1998)

  
 Pidduck  
 (1922)



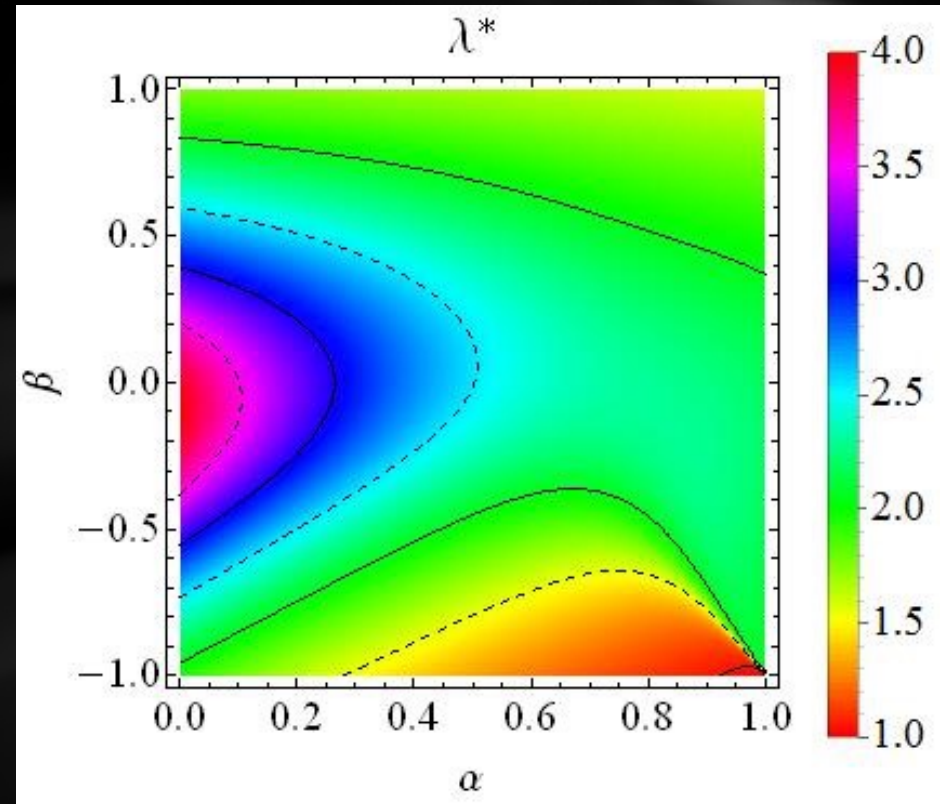
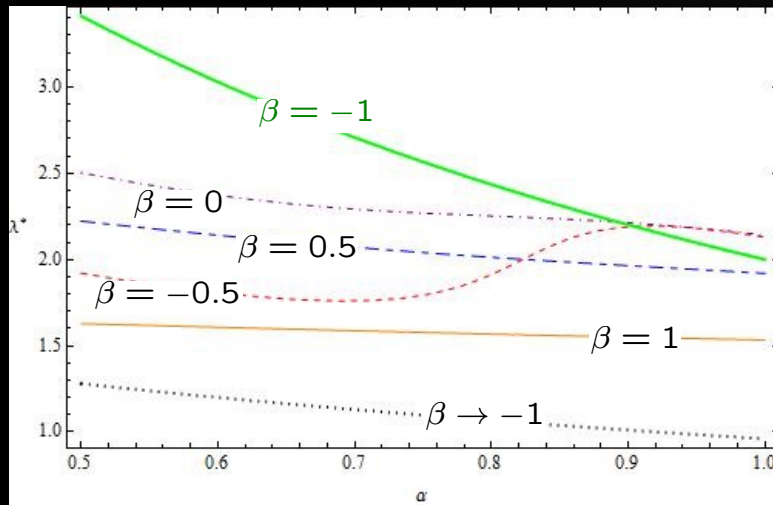
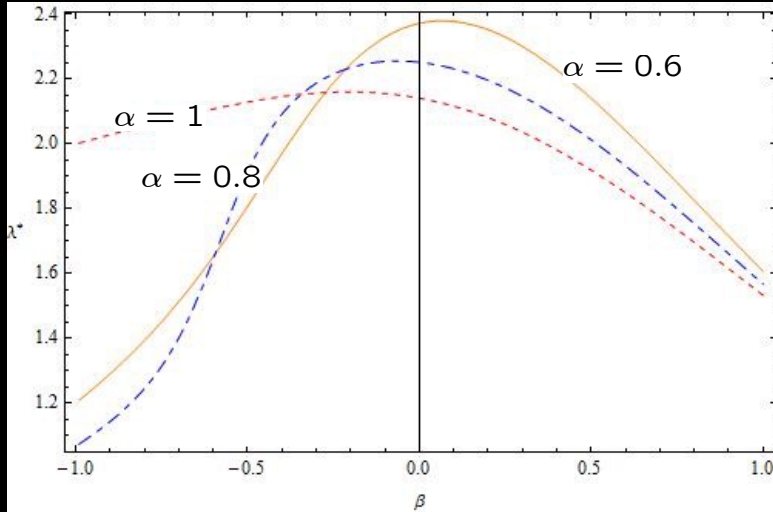
# Shear viscosity

$$P_{ij} = p\delta_{ij} - \eta \left( \nabla_i u_j + \nabla_j u_i - \frac{2}{d} \delta_{ij} \nabla \cdot \mathbf{u} \right) - \eta_b \delta_{ij} \nabla \cdot \mathbf{u}$$



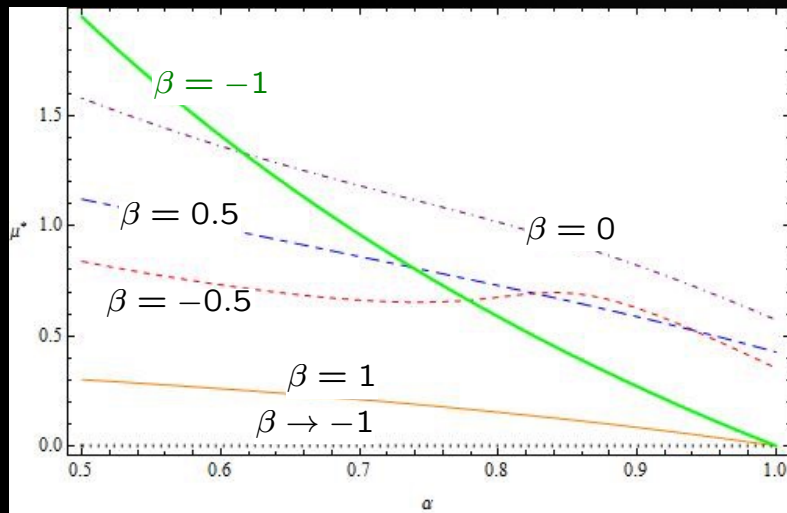
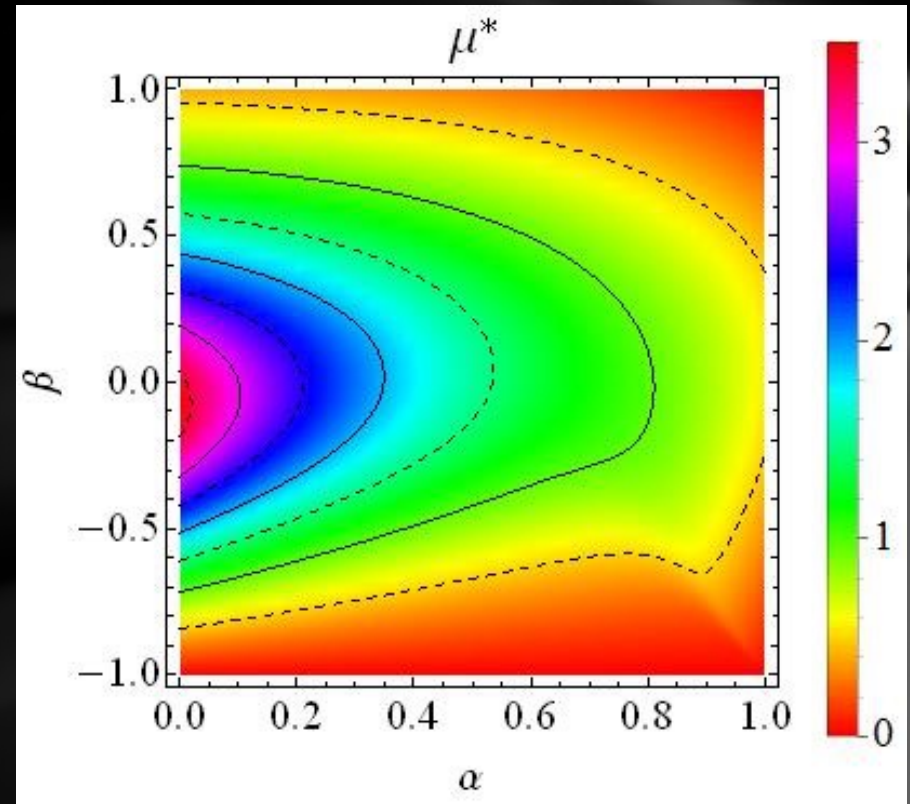
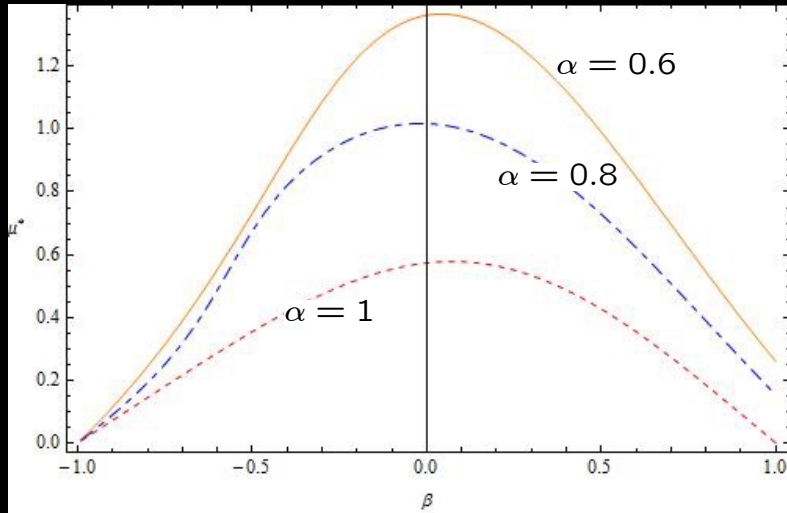
# Thermal conductivity

$$\mathbf{q} = -\lambda \nabla T - \mu \nabla n$$



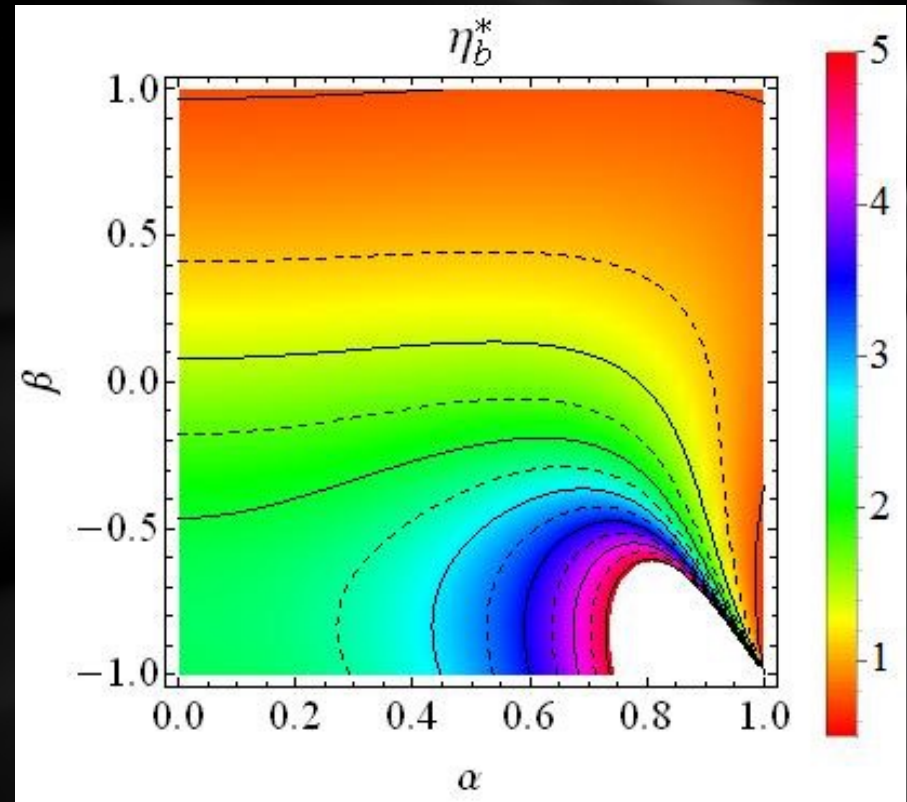
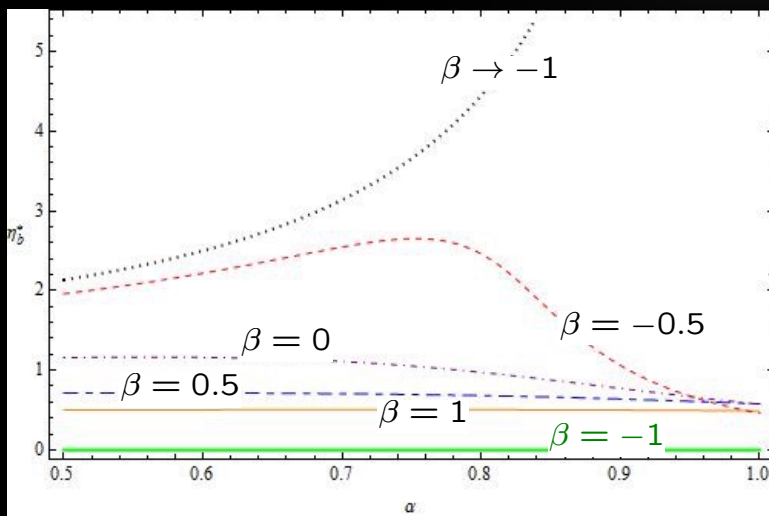
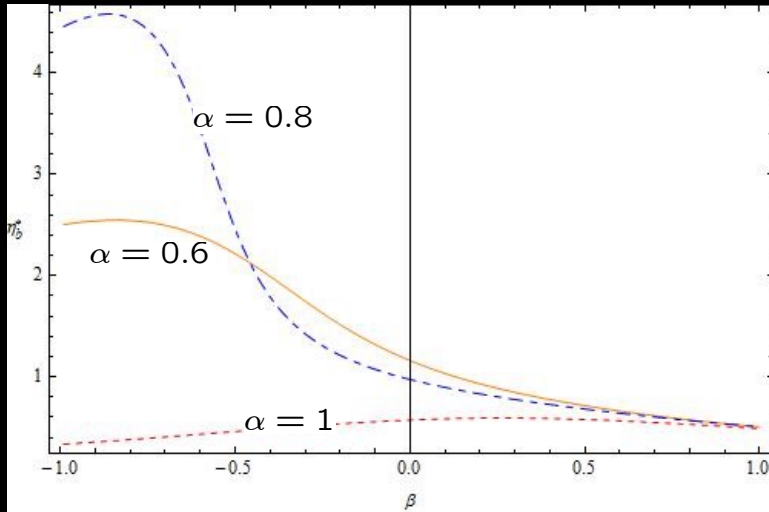
# Dufour-like coefficient

$$\mathbf{q} = -\lambda \nabla T - \mu \nabla n$$



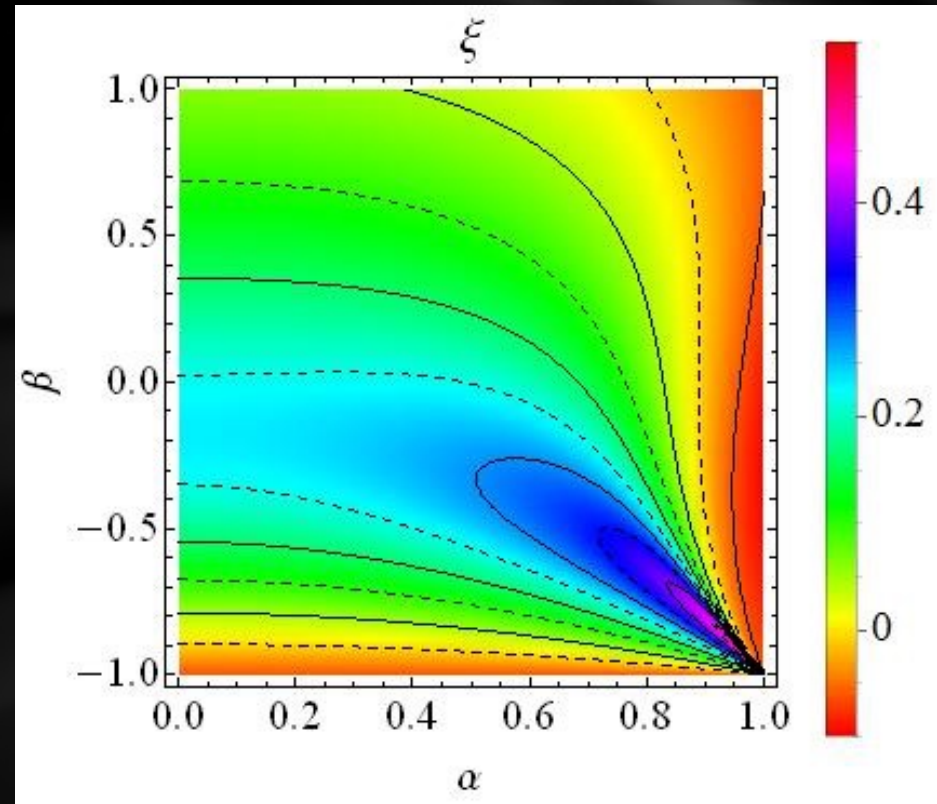
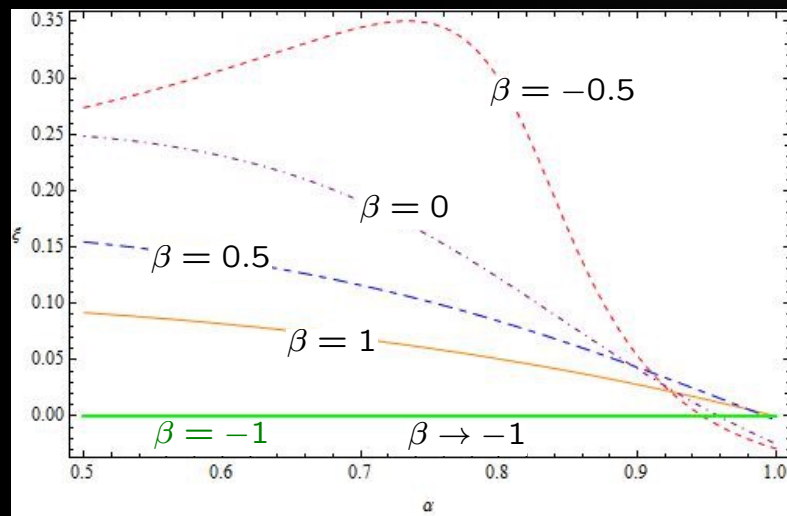
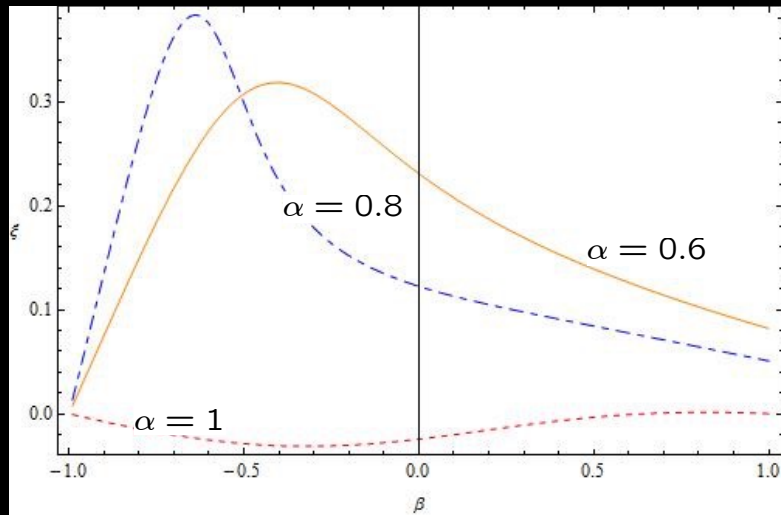
# Bulk viscosity

$$P_{ij} = p\delta_{ij} - \eta \left( \nabla_i u_j + \nabla_j u_i - \frac{2}{d} \delta_{ij} \nabla \cdot \mathbf{u} \right) - \eta_b \delta_{ij} \nabla \cdot \mathbf{u}$$



# Cooling rate coefficient

$$\zeta = \zeta^{(0)} - \xi \nabla \cdot \mathbf{u}$$



# Instability of the Homogeneous Cooling State

*J. Fluid Mech.* (2013), vol. 729, pp. 484–495. © Cambridge University Press 2013  
doi:10.1017/jfm.2013.328 484

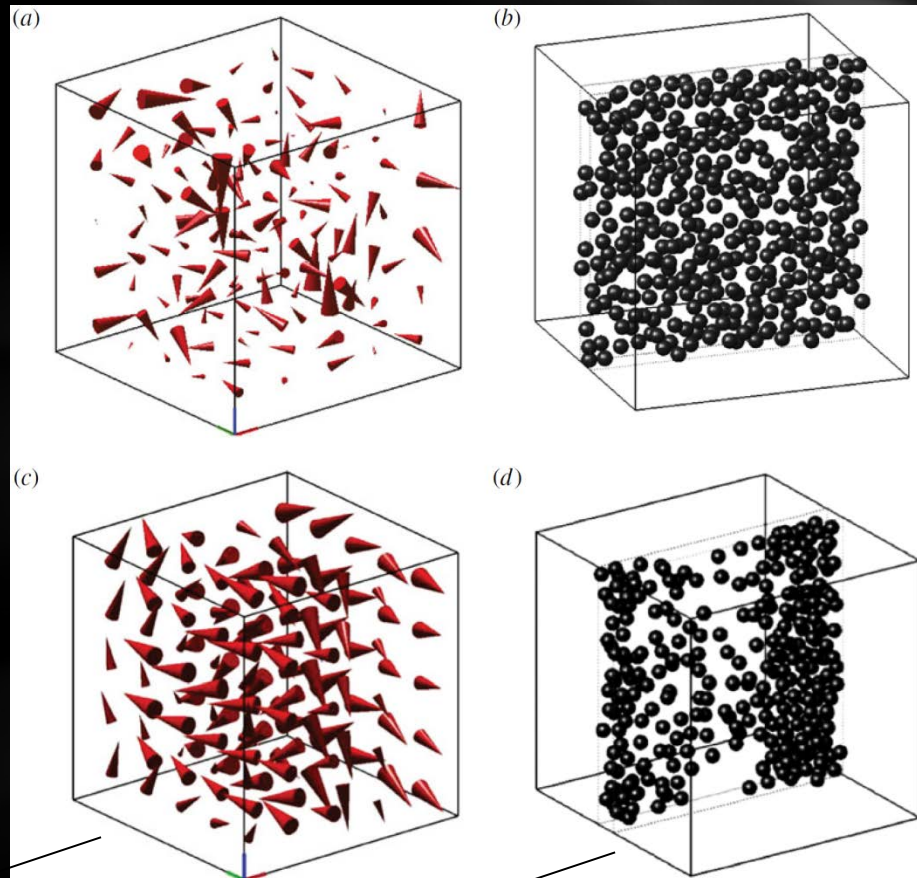
**Dual role of friction in granular flows:  
attenuation versus enhancement of instabilities**

Peter P. Mitrano, Steven R. Dahl, Andrew M. Hilger, Christopher J. Ewasko  
and Christine M. Hrenya†

$$\alpha = 0.7, \quad \beta = -0.7$$

volume fraction  $\phi = 0.3$

$$L/\sigma = 10$$



4 collisions  
per particle

100 collisions  
per particle

Vortices

Clustering

# Linear stability analysis

$$\left. \begin{aligned} n(\mathbf{r}, t) &= n_H [1 + \delta n^*(\mathbf{r}, t)] \\ \mathbf{u}(\mathbf{r}, t) &= \mathbf{u}_H + v_H(t) \delta \mathbf{u}^*(\mathbf{r}, t) \\ T(\mathbf{r}, t) &= T_H(t) [1 + \delta T^*(\mathbf{r}, t)] \end{aligned} \right\} \delta y_\alpha(\mathbf{r}, t), \quad \alpha = 1, \dots, 5$$

Fourier-Laplace transform:

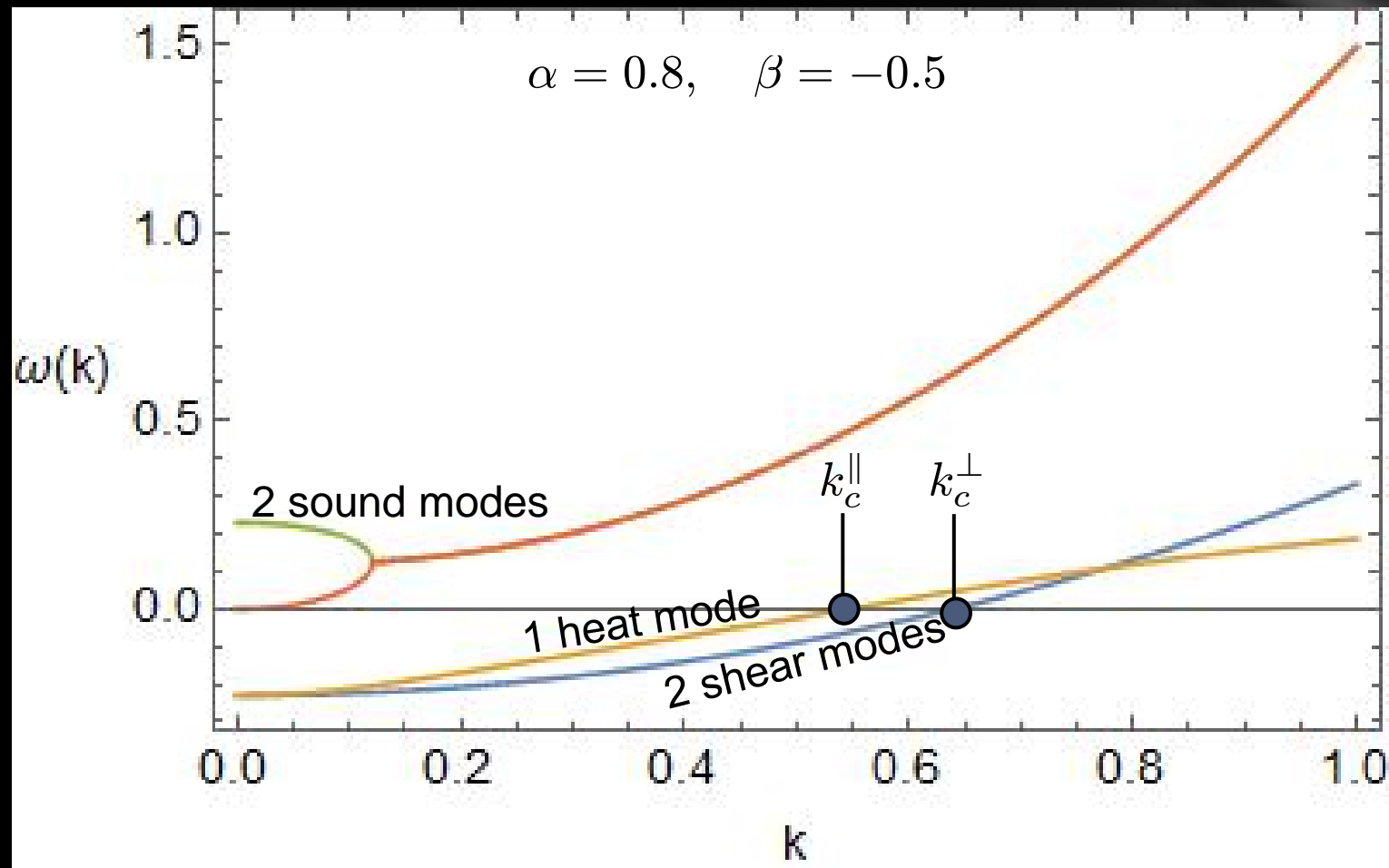
$$\delta y_\alpha(\mathbf{r}, t) = \delta y_{\alpha; \mathbf{k}, \omega} e^{i\mathbf{k} \cdot \mathbf{r}^*} e^{-\omega(k)s} \left[ \mathbf{r}^* \equiv \frac{\mathbf{r}}{\text{m.f.p.}}, \quad s \equiv \frac{1}{2} \int_0^t dt' \nu_H(t') \right]$$

Characteristic equation:

$$\det [\mathbf{M}(k) - \omega(k)\mathbf{I}] = 0 \Rightarrow \text{Dispersion relation}$$

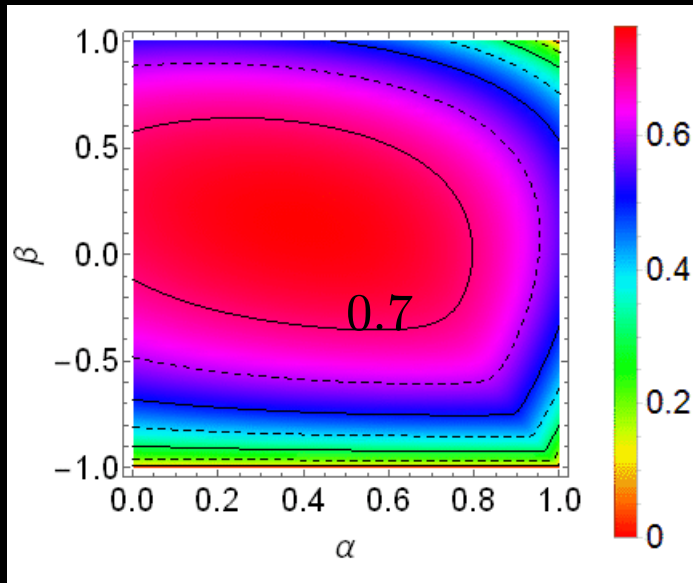
$$\omega(k) < 0 \Rightarrow \text{Instability}$$

# Dispersion relations

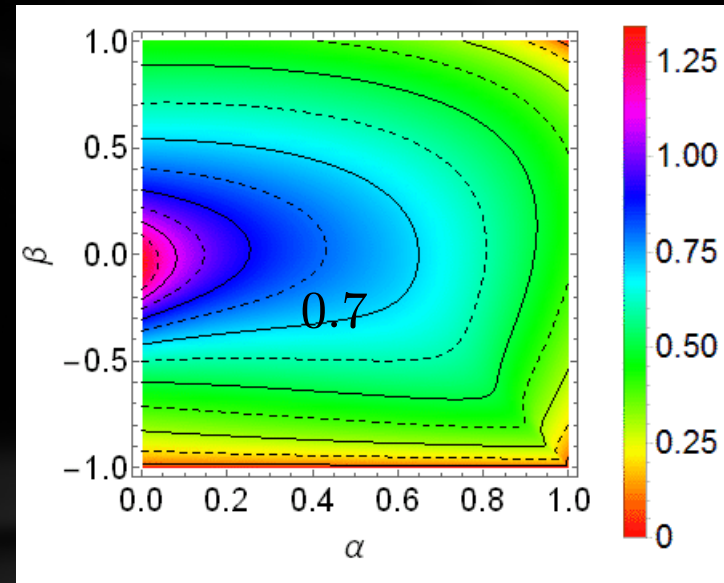




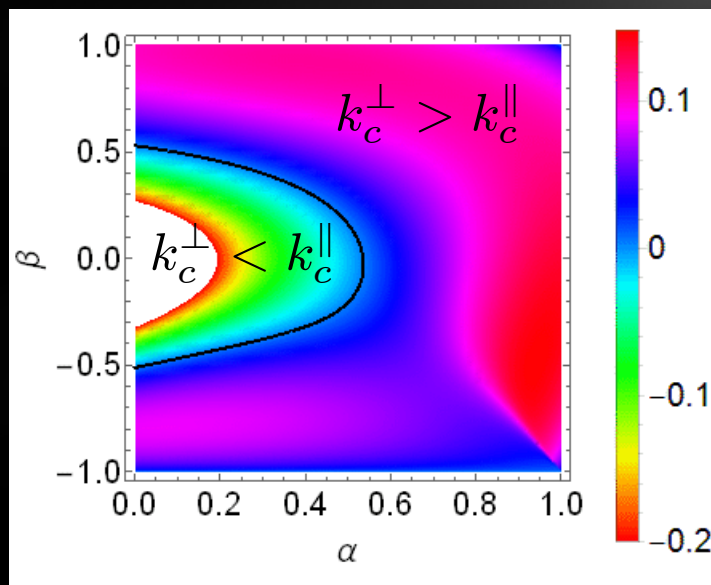
$$k_c^\perp(\alpha, \beta) = \sqrt{2\zeta^*/\eta^*}$$



$$k_c^\parallel(\alpha, \beta) = \sqrt{8\zeta^*/5(\lambda^* - \mu^*)}$$



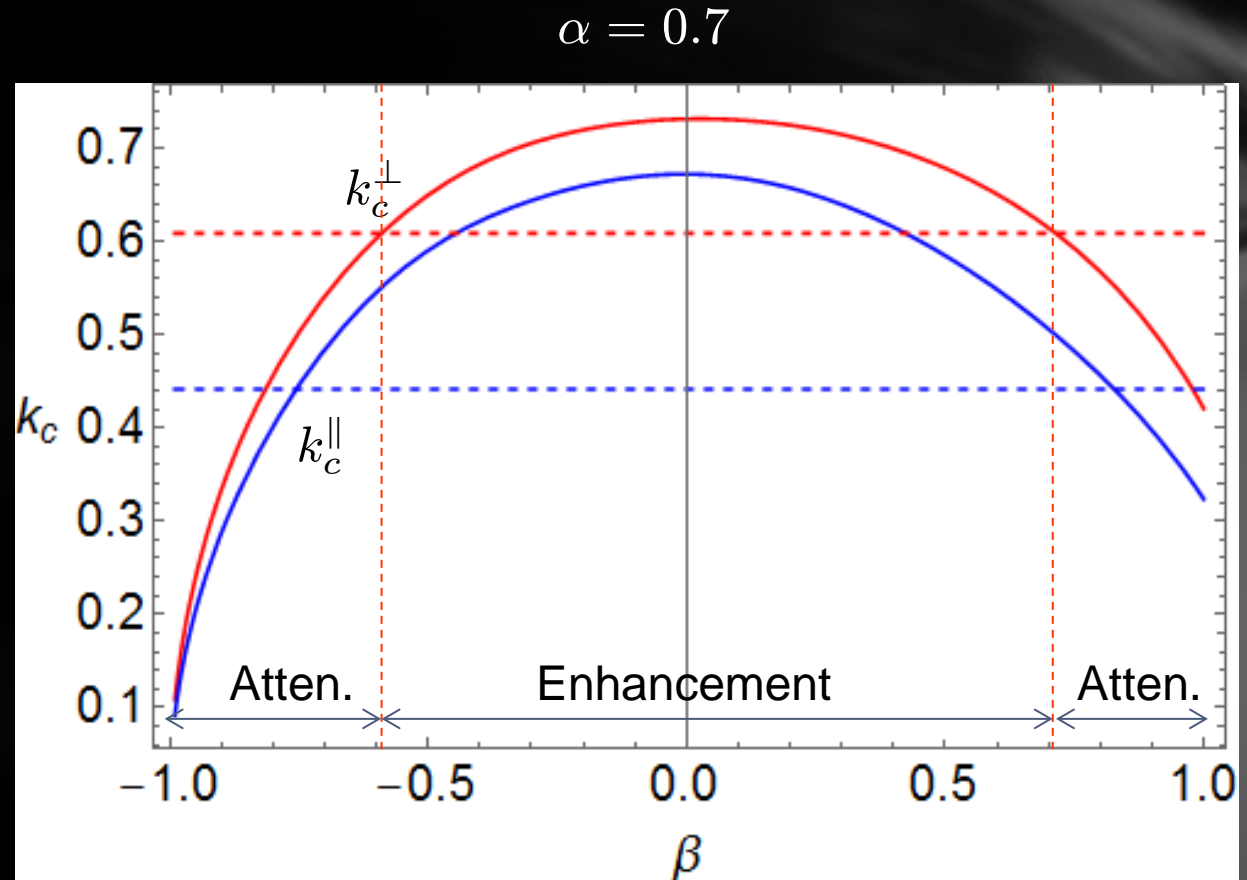
The shear modes (vortices) are more unstable than the heat mode (clusters), except for high inelasticity and medium roughness



$$k_c^\perp(\alpha, \beta) - k_c^\parallel(\alpha, \beta)$$

# Comparison with the pure smooth case

Medium roughness enhances instabilities, while small and high levels of roughness attenuate it

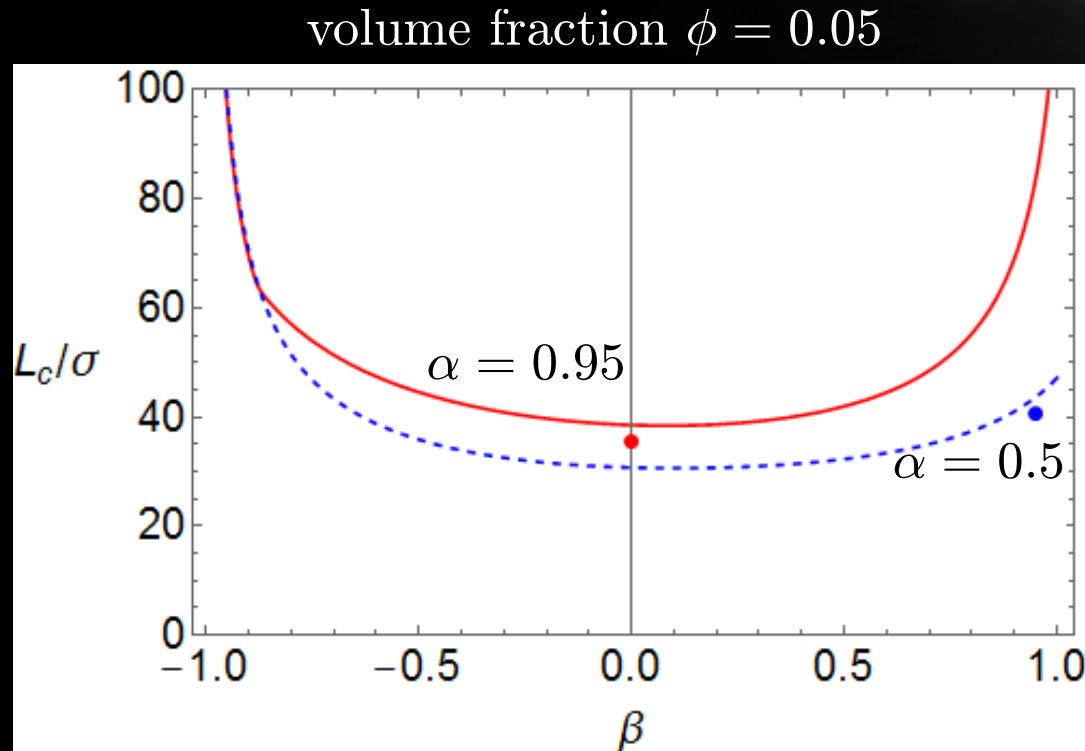


J. Fluid Mech. (2013), vol. 729, pp. 484–495. © Cambridge University Press 2013  
doi:10.1017/jfm.2013.328 484

**Dual** role of friction in granular flows:  
attenuation versus enhancement of instabilities

Peter P. Mitrano, Steven R. Dahl, Andrew M. Hilger, Christopher J. Ewasko  
and Christine M. Hrenya\*

# Comparison with preliminary MD simulations



(MD points, courtesy of Peter Mitrano)

# Outline

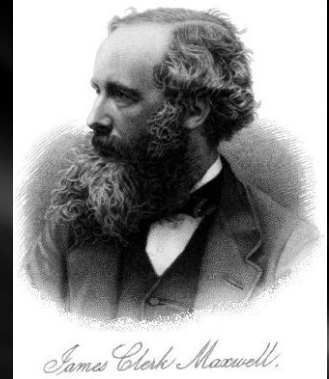
- Introduction. Granular hydrodynamics
- The inelastic rough hard-sphere model (IRHSM). Navier-Stokes coefficients
- The inelastic Maxwell model (IMM)  
Burnett coefficients
- Conclusions

Hydrodynamic  
order ↑

Burnett	<b>2014</b> <b>(<math>dD</math>, Exact)</b>	?	?
Navier-Stokes (NS)	2003 ( $dD$ , Exact)	1998 (Sonine appr.)	<b>2014</b> <b>(3D, Sonine appr.)</b>
	Inelastic Maxwell model (IMM)	Inelastic smooth hard-sphere model (ISHSM)	Inelastic rough hard-sphere model (IRHSM)

→ Model complexity

# Inelastic Maxwell model (IMM)



*James Clerk Maxwell,*

(1831–1879)

- First proposed by Bobylev, Carrillo & Gamba (2000), Ben-Naim & Krapivsky (2000), Bobylev & Cercignani (2002), Ernst & Brito (2002), ...
- The hard-sphere collision rate (proportional to the *relative velocity*) is replaced by an effective (mean-field) *constant* value.
- Otherwise, the collision rule remains unchanged.

# Inelastic Maxwell model (IMM)

Boltzmann eq.:

$$\partial_t f(\mathbf{r}, \mathbf{v}, t) + \mathbf{v} \cdot \nabla f(\mathbf{r}, \mathbf{v}, t) = J[\mathbf{r}, \mathbf{v}, t|f]$$

ISHSM:

$$J[\mathbf{v}_1|f] = \sigma^{d-1} \int d\mathbf{v}_2 \int d\hat{\boldsymbol{\sigma}} \Theta(\mathbf{g} \cdot \hat{\boldsymbol{\sigma}}) (\mathbf{g} \cdot \hat{\boldsymbol{\sigma}}) [\alpha^{-2} f(\mathbf{v}'_1) f(\mathbf{v}'_2) - f(\mathbf{v}_1) f(\mathbf{v}_2)]$$

IMM:

$$J[\mathbf{v}_1|f] = \frac{d+2}{2\Omega_d} \frac{\nu}{n} \int d\mathbf{v}_2 \int d\hat{\boldsymbol{\sigma}} [\alpha^{-1} f(\mathbf{v}'_1) f(\mathbf{v}'_2) - f(\mathbf{v}_1) f(\mathbf{v}_2)],$$

$$\nu \propto T^\gamma, \quad \gamma = \frac{1}{2}$$

# Exact moments

Collisional moment of order  $k$  = Linear combination of velocity moments of order equal to or smaller than  $k$

$$m \int d\mathbf{v} V_i V_j J[\mathbf{v}, f] = -\nu_{0|2}(\alpha) (P_{ij} - p\delta_{ij}) - \zeta(\alpha) p\delta_{ij}$$

$$\frac{m}{2} \int d\mathbf{v} V^2 V_i J[\mathbf{v}, f] = -\nu_{2|1}(\alpha) q_i$$

$$\dots = \dots$$



# Results

$$\begin{aligned}
 P_{ij}^{(2)} = & a_1 \frac{\lambda_0}{\nu} \left( \nabla_i \nabla_j T - \frac{1}{d} \delta_{ij} \nabla^2 T \right) + a_2 \frac{T \lambda_0}{p \nu} \left( \nabla_i \nabla_j p - \frac{1}{d} \delta_{ij} \nabla^2 p \right) \\
 & a_3 \frac{\lambda_0}{T \nu} \left[ \nabla_i T \nabla_j T - \frac{1}{d} \delta_{ij} (\nabla T)^2 \right] + a_4 \frac{T \lambda_0}{p^2 \nu} \left[ \nabla_i p \nabla_j p - \frac{1}{d} \delta_{ij} (\nabla p)^2 \right] \\
 & + a_5 \frac{\lambda_0}{p \nu} \left( \nabla_i T \nabla_j p + \nabla_i p \nabla_j T - \frac{2}{d} \delta_{ij} \nabla p \cdot \nabla T \right) + a_6 \frac{\eta_0}{\nu} D \left( D_{ij} - \frac{1}{d} \delta_{ij} D \right) \\
 & + a_7 \frac{\eta_0}{\nu} \left[ D_{ik} D_{kj} - \omega_{ik} \omega_{kj} - \frac{1}{d} \delta_{ij} (D_{lk} D_{kl} - \omega_{lk} \omega_{kl}) + \omega_{ij} D_{kj} - D_{ik} \omega_{kj} \right] \\
 q_i^{(2)} = & b_1 \frac{T \lambda_0}{\nu} \nabla^2 u_i + b_2 \frac{T \lambda_0}{\nu} \nabla_i D + b_3 \frac{\lambda_0}{\nu} D_{ij} \nabla_j T + b_4 \frac{\eta_0}{\rho \nu} D_{ij} \nabla_j p + b_5 \frac{\lambda_0}{\nu} \omega_{ij} \nabla_j T \\
 & + b_6 \frac{\eta_0}{\rho \nu} \omega_{ij} \nabla_j p + b_7 \frac{\lambda_0}{\nu} D \nabla_i T + b_8 \frac{\eta_0}{\rho \nu} D \nabla_i p,
 \end{aligned}$$

$$D \equiv \nabla \cdot \mathbf{u}, \quad D_{ij} \equiv \frac{1}{2} (\nabla_i u_j + \nabla_j u_i), \quad \omega_{ij} \equiv \frac{1}{2} (\nabla_j u_i - \nabla_i u_j)$$

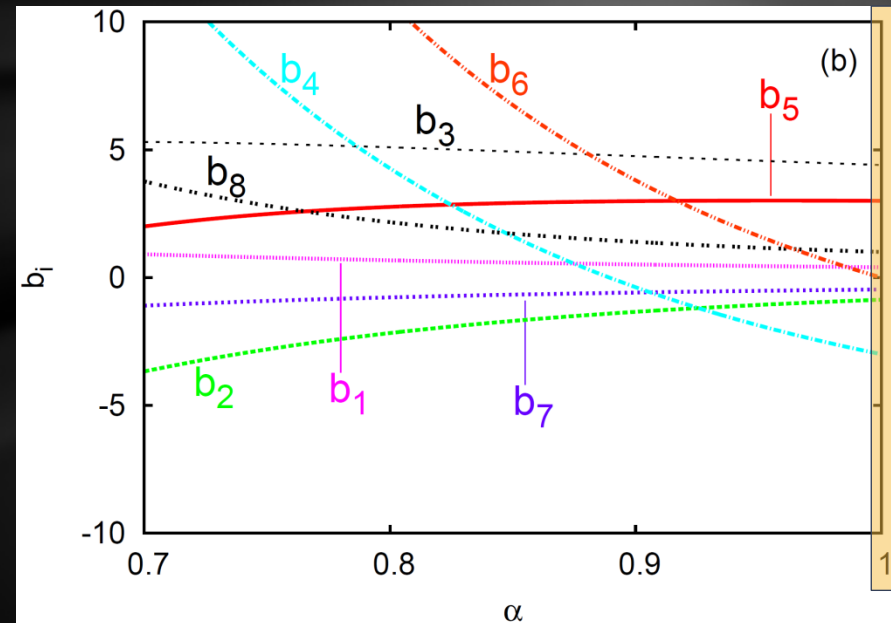
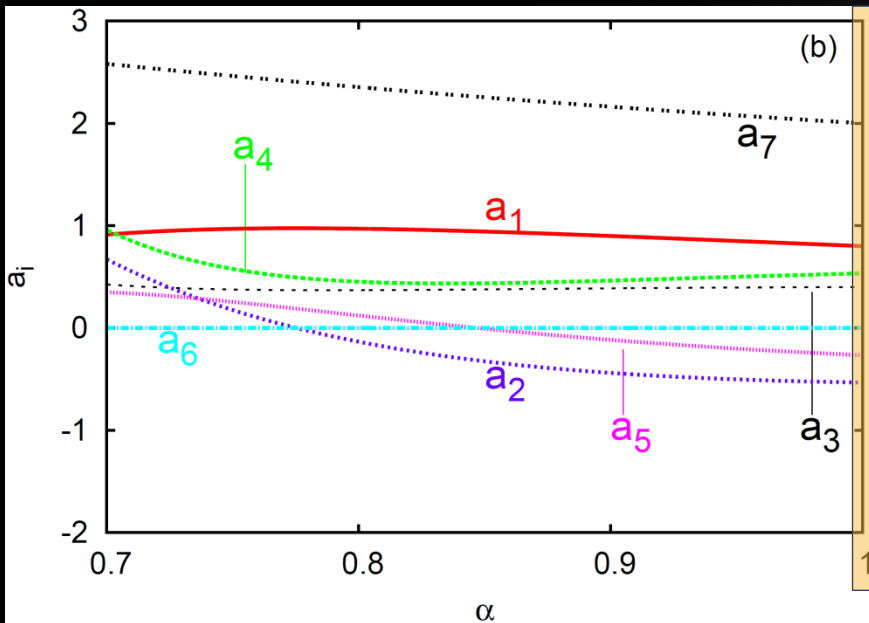
# Elastic limit ( $\alpha \rightarrow 1$ )

$$\begin{aligned} a_1 &\rightarrow \frac{4}{d+2}, & a_2 &\rightarrow -\frac{4(d-1)}{d(d+2)}, & a_3 &\rightarrow \frac{4(1-\gamma)}{d+2}, & a_4 &\rightarrow \frac{4(d-1)}{d(d+2)}, \\ a_5 &\rightarrow -\frac{2(d-1)}{d(d+2)}, & a_6 &\rightarrow \frac{2(d-4+2\gamma)}{d}, & a_7 &\rightarrow 2, & & \\ b_1 &\rightarrow \frac{2}{d+2}, & b_2 &\rightarrow -\frac{2(5d-2)}{d(d-1)(d+2)}, & b_3 &\rightarrow \frac{2[d^2+7d-6-2(d-1)\gamma]}{(d-1)(d+2)}, & b_4 &\rightarrow -\frac{2d}{d-1}, \\ b_5 &\rightarrow \frac{2d}{d-1}, & b_6 &\rightarrow 0, & b_7 &\rightarrow \frac{d^3-2d^2-18d+12+2(d^2+4d-2)\gamma}{d(d-1)(d+2)}, & b_8 &\rightarrow \frac{2}{d-1} \end{aligned}$$

- Exact results for Maxwell molecules if  $\gamma = 0$ .
- First Sonine approximation for any potential if  $\gamma = 1 - \partial \ln \eta_0(T) / \partial \ln T$ .
- Generalization to any  $d$  of Chapman & Cowling's classical expressions ( $d = 3$ ).

# Influence of inelasticity (IMM, exact)

$$d = 3, \gamma = \frac{1}{2}$$



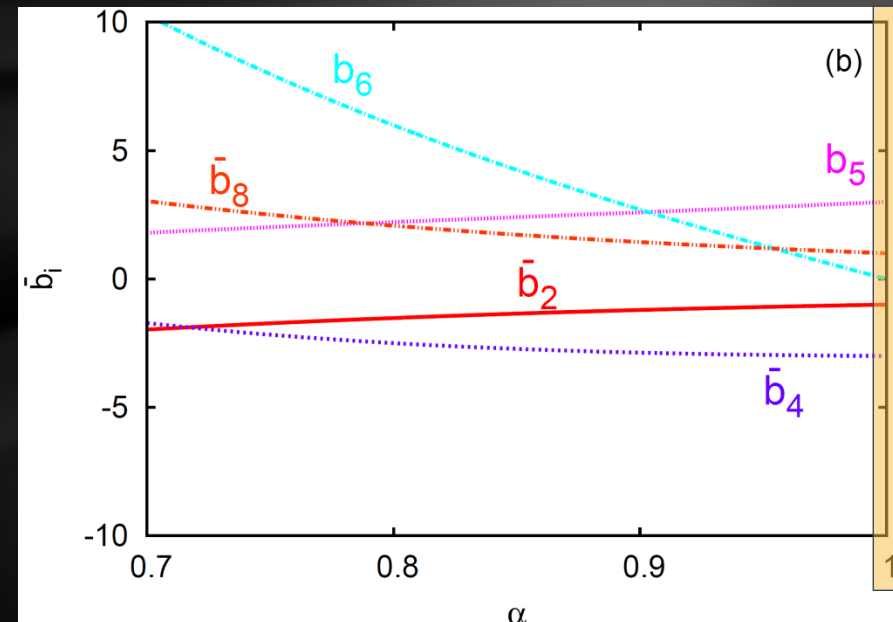
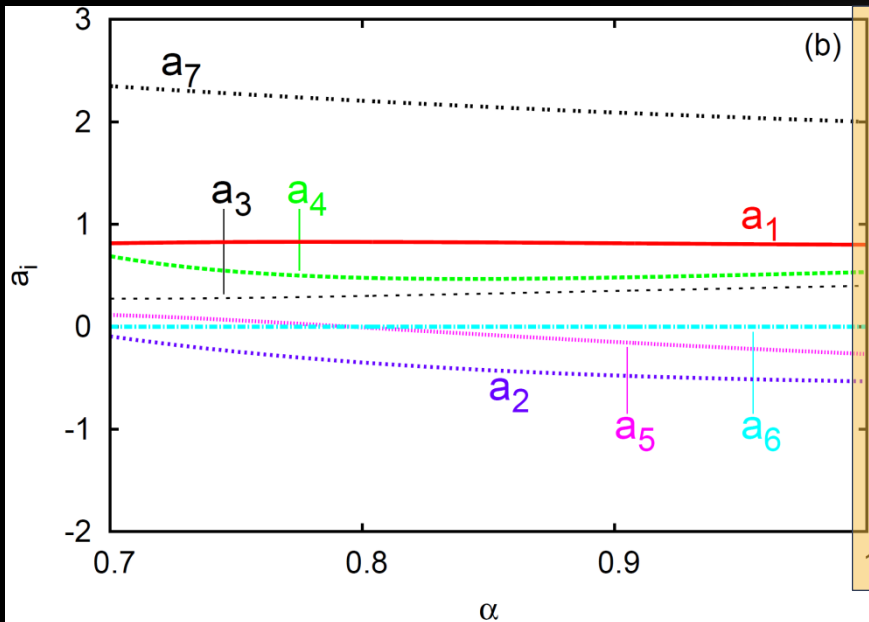
Hydrodynamic  
order ↑

Burnett	2014 ( $dD$ , Exact)	?	?
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	Inelastic Maxwell model (IMM)	Inelastic smooth hard-sphere model (ISHSM)	Inelastic rough hard-sphere model (IRHSM)

→ Model complexity

# Influence of inelasticity (ISHSM, estimated)

$$d = 3$$



# Outline

- Introduction. Granular hydrodynamics
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Burnett coefficients
- Conclusions



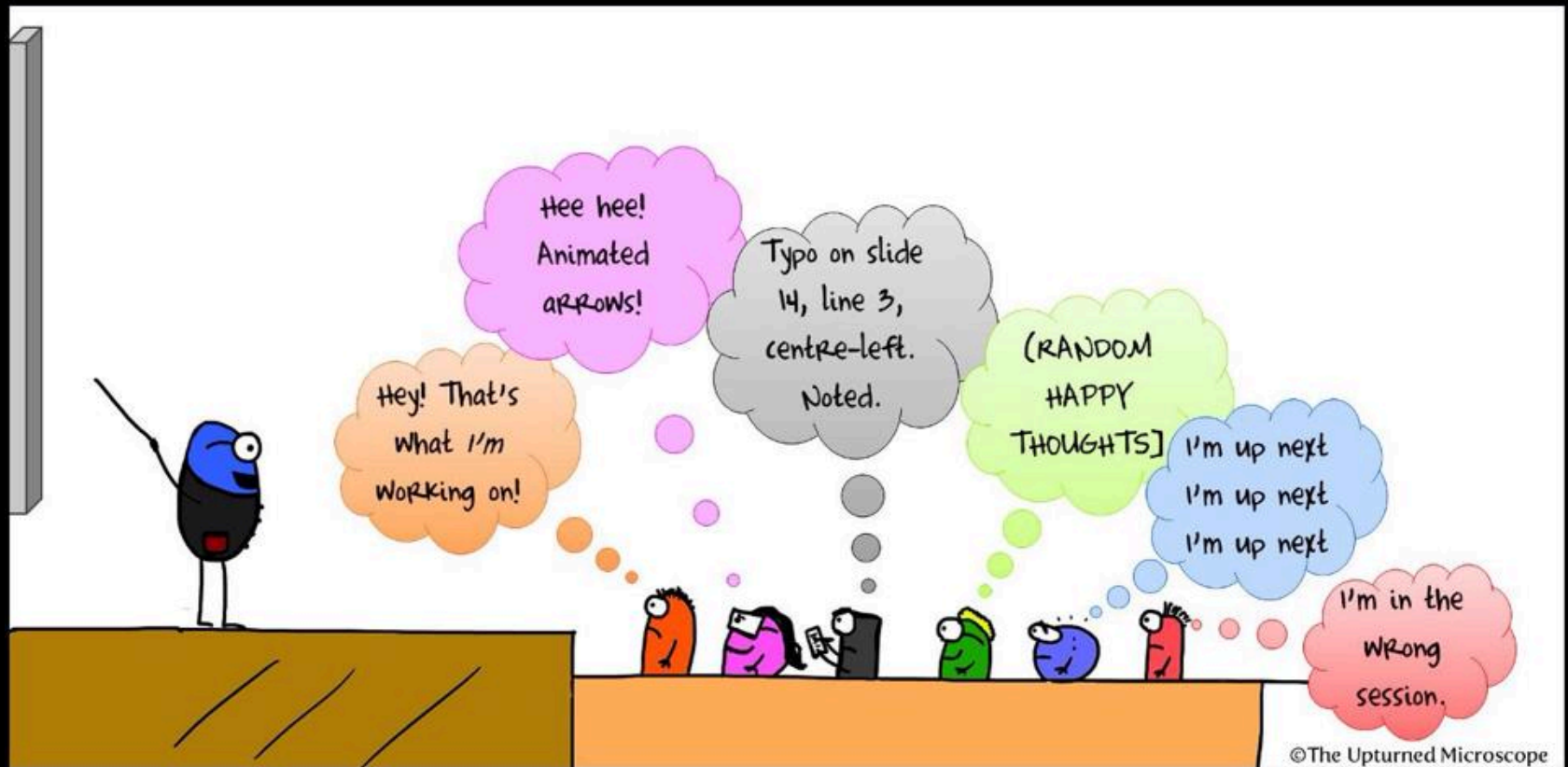
THE

# TAKE-HOME MESSAGE

- **IRHSM:** Roughness (and inelasticity) have a large impact on the NS transport coefficients.
- **IMM:** *Exact* results for the Burnett coefficients can be obtained. They can be used to estimate the coefficients for the ISHSM.

THANK  
YOU!

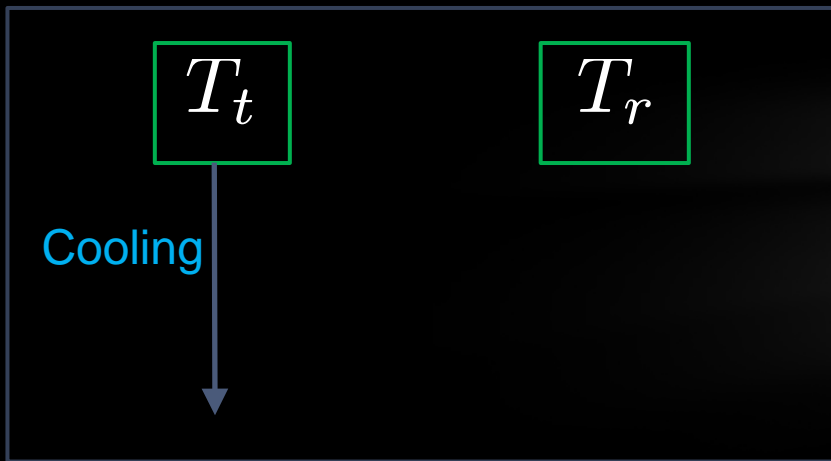
What people think about  
during your conference talk





# Origin of the singular behavior in the quasi-smooth limit

$$\beta = -1$$



$$\beta \gtrsim -1$$

