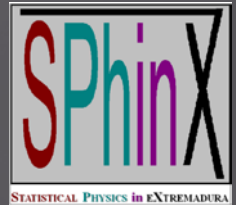


HYDRODYNAMICS FOR A GRANULAR GAS OF INELASTIC ROUGH HARD SPHERES

Andrés Santos

Universidad de Extremadura, Badajoz, Spain



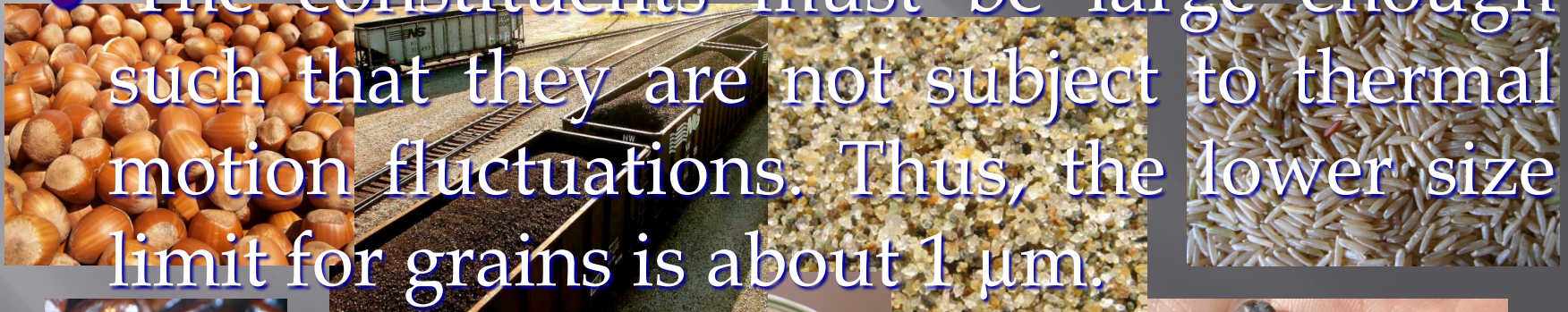
In collaboration with

- V. Garzó (Badajoz, Spain)
- G. M. Kremer (Curitiba, Brazil)



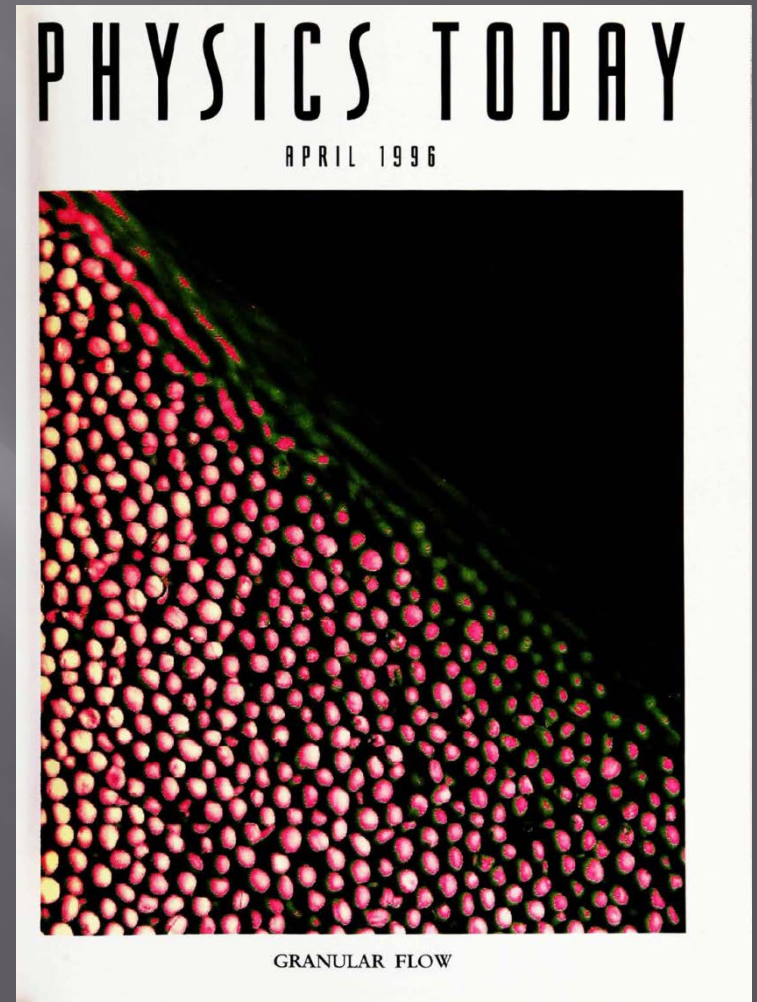
What is a granular material?

- It is a conglomeration of discrete solid, macroscopic particles characterized by a loss of energy whenever the grains collide.
- The constituents must be large enough such that they are not subject to thermal motion fluctuations. Thus, the lower size limit for grains is about $1 \mu\text{m}$.

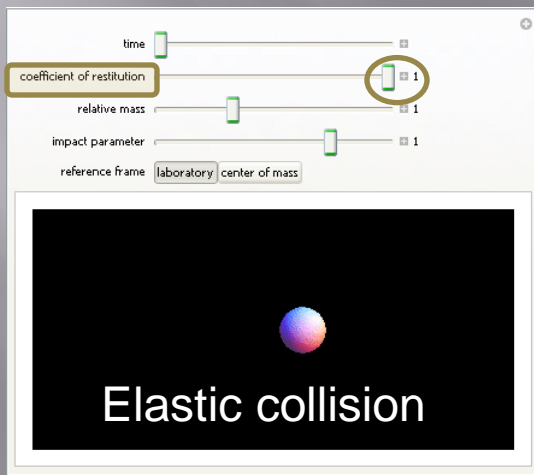


What is a granular *fluid*?

- ▣ When the granular matter is driven and energy is fed into the system (e.g., by shaking) such that the grains are not in constant contact with each other, the granular material is said to *fluidize*.



Minimal model of a granular gas: A gas of *identical smooth inelastic* hard spheres



time

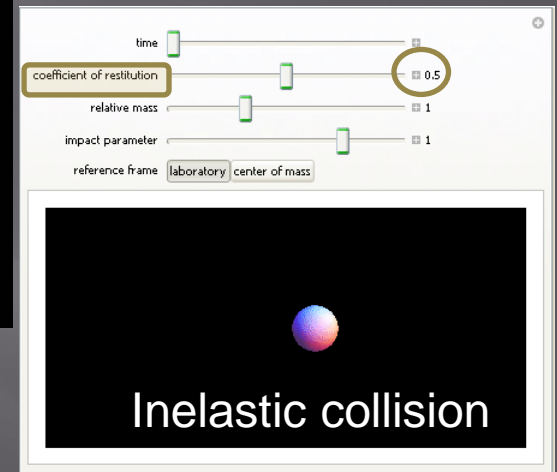
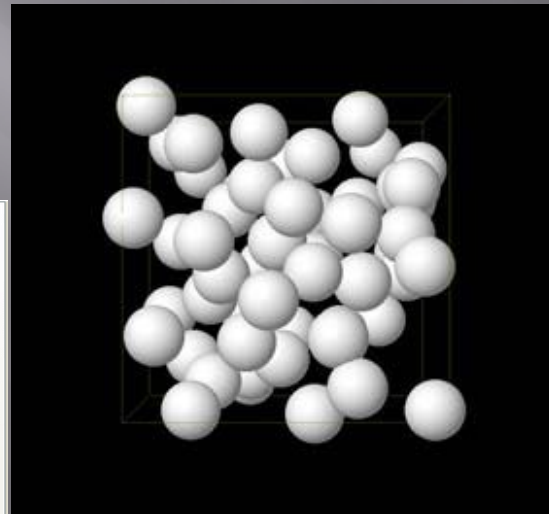
coefficient of restitution 1

relative mass 1

impact parameter 1

reference frame laboratory center of mass

Elastic collision



time

coefficient of restitution 0.5

relative mass 1

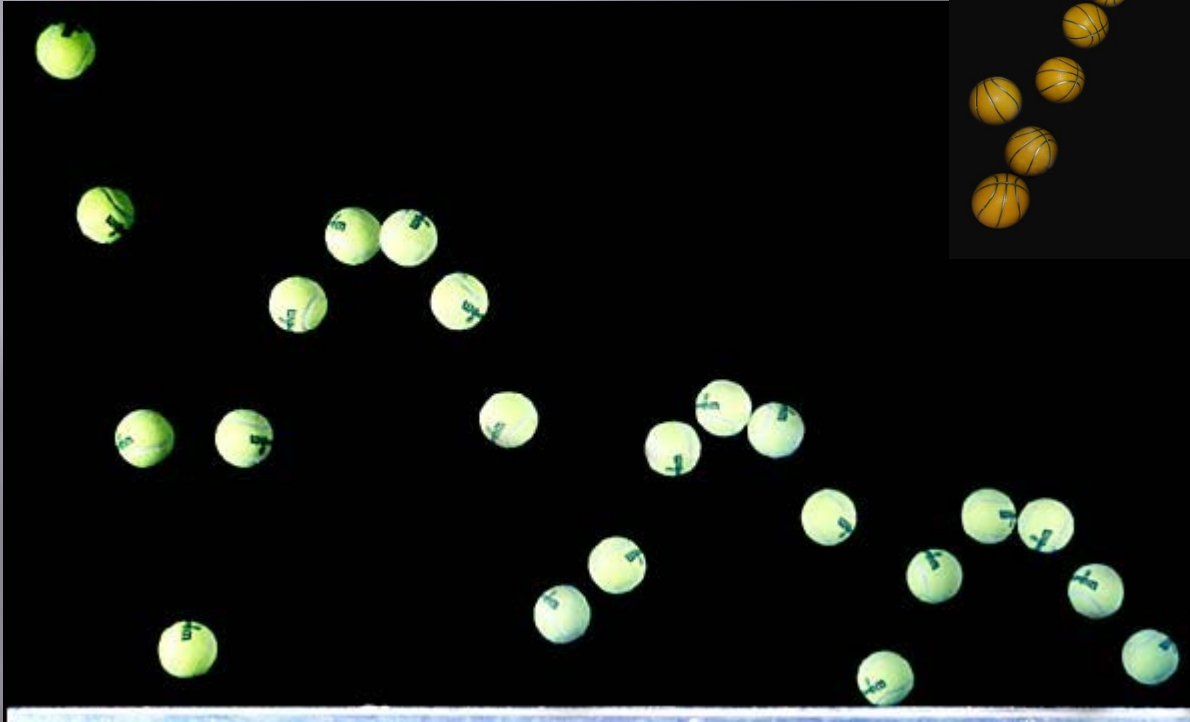
impact parameter 1

reference frame laboratory center of mass

Inelastic collision

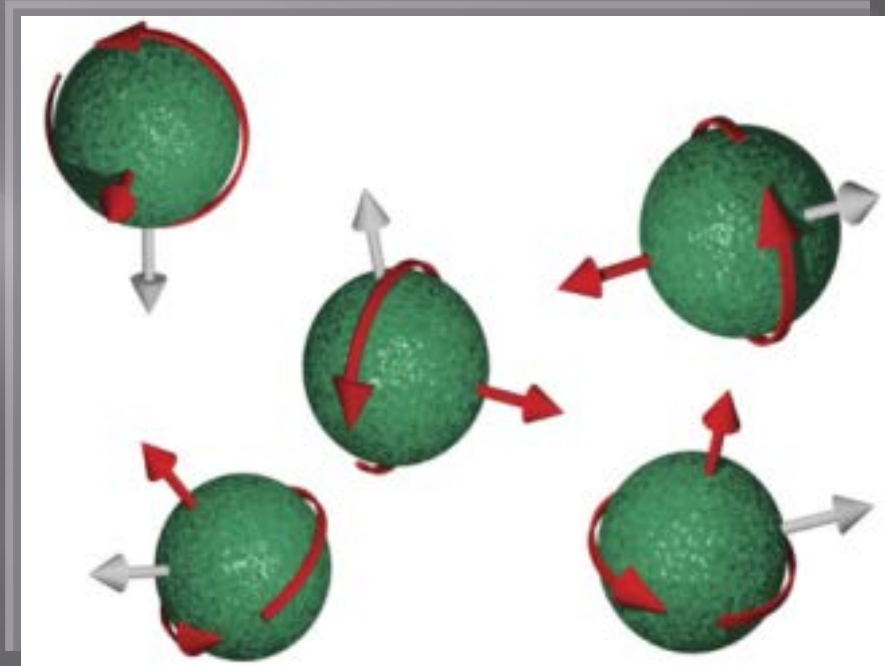
<http://demonstrations.wolfram.com/InelasticCollisionsOfTwoSpheres/>

But this minimal model ignores
roughness (spinning)



Simple model of a granular gas: *A collection of inelastic **rough** hard spheres*

This model unveils an inherent breakdown of energy equipartition in granular fluids, even in homogeneous and isotropic states



N. V. Brilliantov, T. Pöschel, W. T. Kranz, and A. Zippelius,
Phys. Rev. Lett. **98**, 128001 (2007)

Outline of the talk

- ▣ 0. Collision rules for inelastic rough hard spheres
- ▣ 1. Navier-Stokes-Fourier transport coefficients
- ▣ 2. Stability analysis
- ▣ 3. Conclusions

Outline of the talk

- ▣ 0. Collision rules for inelastic rough hard spheres
- ▣ 1. Navier-Stokes-Fourier transport coefficients.
- ▣ 2. Stability analysis
- ▣ 3. Conclusions

Material parameters:

- Mass m
- Diameter σ
- Moment of inertia I ($\kappa=4I/m\sigma^2$)
- Coefficient of normal restitution α
- Coefficient of tangential restitution β
- $\alpha=1$ for perfectly elastic particles
- $\beta=-1$ for perfectly smooth particles
- $\beta=+1$ for perfectly rough particles

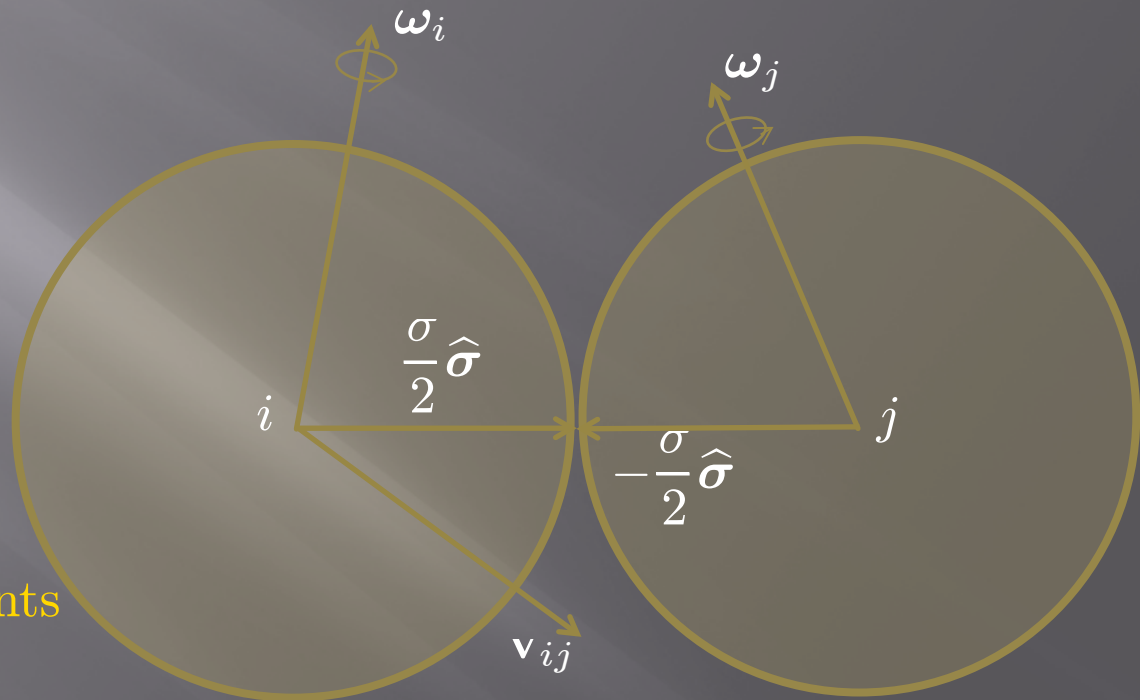
Collision rules

Cons. linear momentum:

$$\mathbf{v}'_i + \mathbf{v}'_j = \mathbf{v}_i + \mathbf{v}_j$$

Cons. angular momentum:

$$\begin{aligned} I\boldsymbol{\omega}'_{i,j} \mp m\frac{\sigma_i}{2}\hat{\boldsymbol{\sigma}} \times \mathbf{v}'_{i,j} \\ = I\boldsymbol{\omega}_{i,j} \mp m\frac{\sigma_i}{2}\hat{\boldsymbol{\sigma}} \times \mathbf{v}_{i,j} \end{aligned}$$



Relative velocity of the points of the spheres at contact:

$$\bar{\mathbf{v}}_{ij} = \mathbf{v}_{ij} - \frac{\sigma}{2}\hat{\boldsymbol{\sigma}} \times (\boldsymbol{\omega}_i + \boldsymbol{\omega}_j)$$

$$\left| \hat{\boldsymbol{\sigma}} \cdot \bar{\mathbf{v}}'_{ij} = -\alpha \hat{\boldsymbol{\sigma}} \cdot \bar{\mathbf{v}}_{ij}, \quad \hat{\boldsymbol{\sigma}} \times \bar{\mathbf{v}}'_{ij} = -\beta \hat{\boldsymbol{\sigma}} \times \bar{\mathbf{v}}_{ij} \right|$$

Energy collisional loss

$$E_{ij} = \frac{1}{2}mv_i^2 + \frac{1}{2}mv_j^2 + \frac{1}{2}I\omega_i^2 + \frac{1}{2}I\omega_j^2$$

$$E'_{ij} - E_{ij} = -(1 - \alpha^2) \times \dots \\ -(1 - \beta^2) \times \dots$$

Energy is conserved *only* if the spheres are

- perfectly elastic ($\alpha=1$) and
- either
 - perfectly smooth ($\beta=-1$) or
 - perfectly rough ($\beta=+1$)

coefficient of normal restitution 1

coefficient of tangential restitution -1

relative mass 1


impact parameter 0

initial angular velocity of the left particle 1

time -10

reference frame laboratory center of mass

energy loss (lab frame) = 0%




Elastic & smooth

<http://demonstrations.wolfram.com/InelasticCollisionsOfTwoRoughSpheres/>

coefficient of normal restitution 0.5
coefficient of tangential restitution -1
relative mass 1
impact parameter 0
initial angular velocity of the left particle 1
time -10
reference frame laboratory center of mass

energy loss (lab frame) = 27%



Inelastic & smooth

<http://demonstrations.wolfram.com/InelasticCollisionsOfTwoRoughSpheres/>

coefficient of normal restitution 1

coefficient of tangential restitution 1

relative mass 1


impact parameter 0

initial angular velocity of the left particle 1

time -10

reference frame laboratory center of mass

energy loss (lab frame) = 0%




Elastic & (perfectly) rough

<http://demonstrations.wolfram.com/InelasticCollisionsOfTwoRoughSpheres/>

coefficient of normal restitution 0.5
coefficient of tangential restitution 1
relative mass 1
impact parameter 0
initial angular velocity of the left particle 1
time -10
reference frame laboratory center of mass

energy loss (lab frame) = 27%



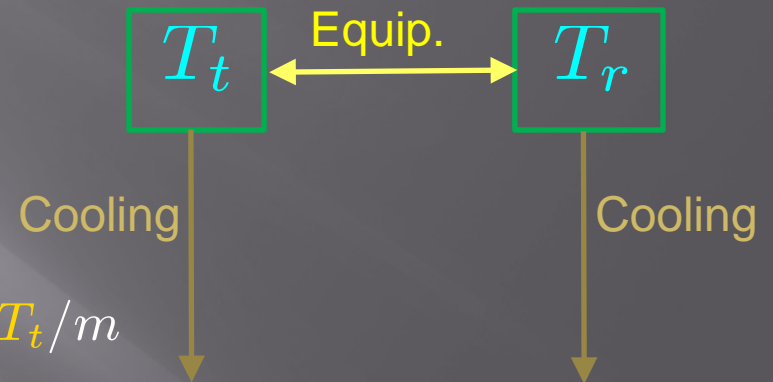
Inelastic & (perfectly) rough

<http://demonstrations.wolfram.com/InelasticCollisionsOfTwoRoughSpheres/>

Outline of the talk

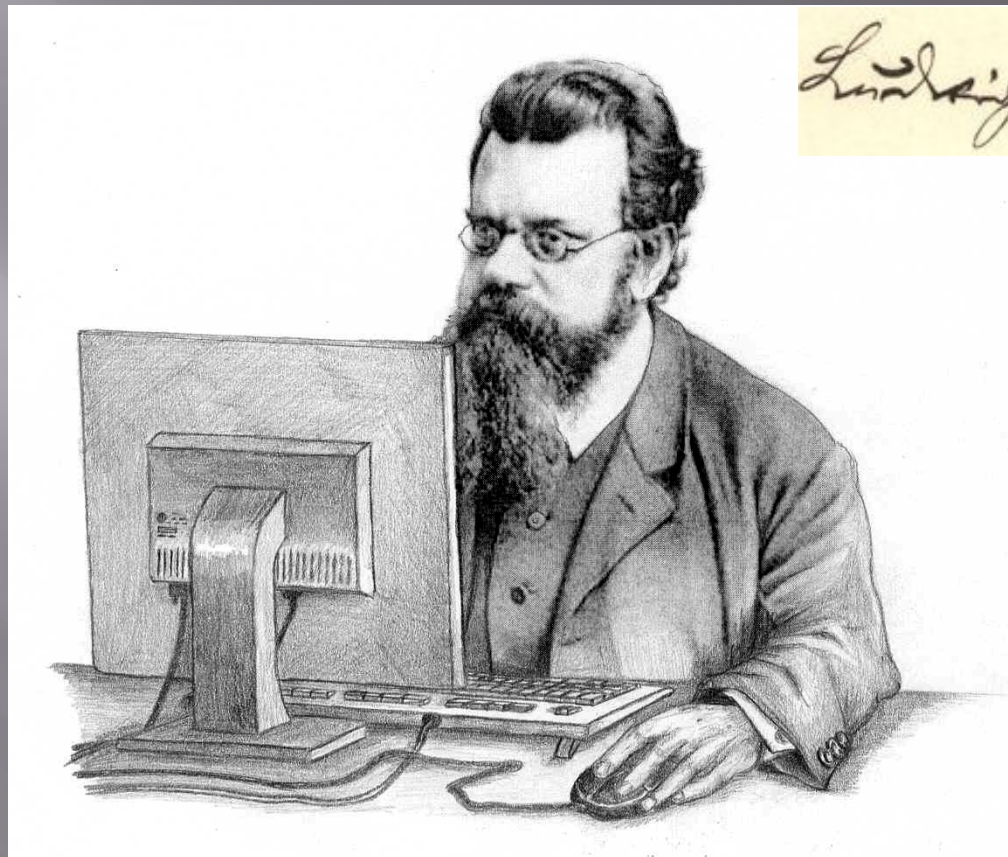
- ▣ 0. Collision rules for inelastic rough hard spheres
- ▣ 1. Navier-Stokes-Fourier transport coefficients
- ▣ 2. Stability analysis
- ▣ 3. Conclusions

Homogeneous Cooling State (HCS)



- Translational temperature: $\langle (\mathbf{v} - \mathbf{u})^2 \rangle = 3T_t/m$
- Rotational temperature: $\langle \omega^2 \rangle = 3T_r/I$
- Temperature ratio: $\theta \equiv T_r/T_t$

$$T_t(t) \sim t^{-2}, \quad T_r(t)/T_t(t) \rightarrow \text{const} \neq 1$$



Ludwig Boltzmann

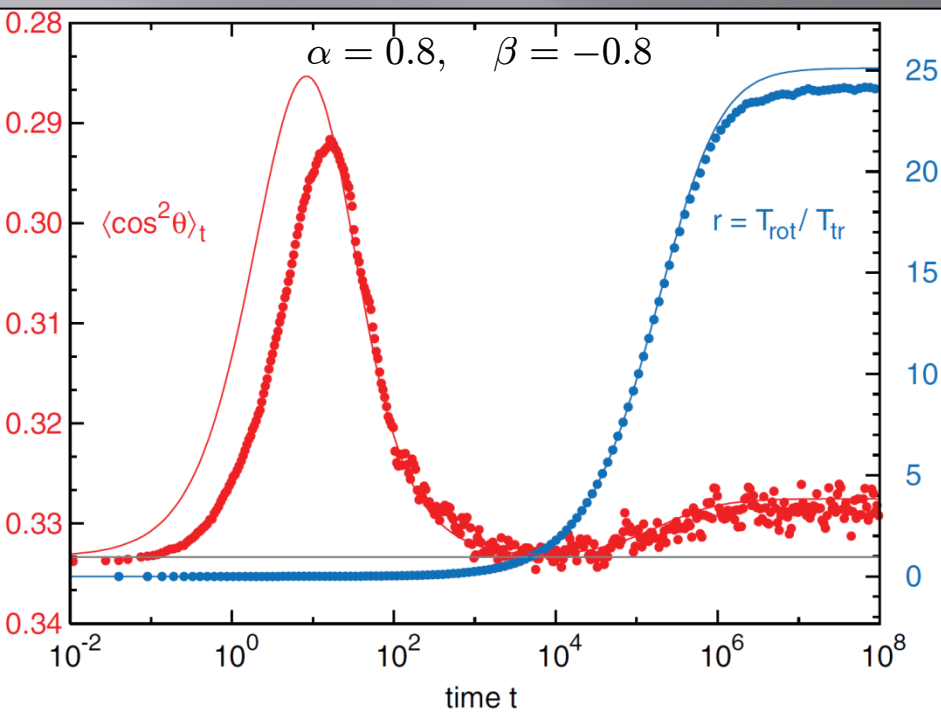
(1844-1906)

(Cartoon by Bernhard Reischl, University of Vienna)

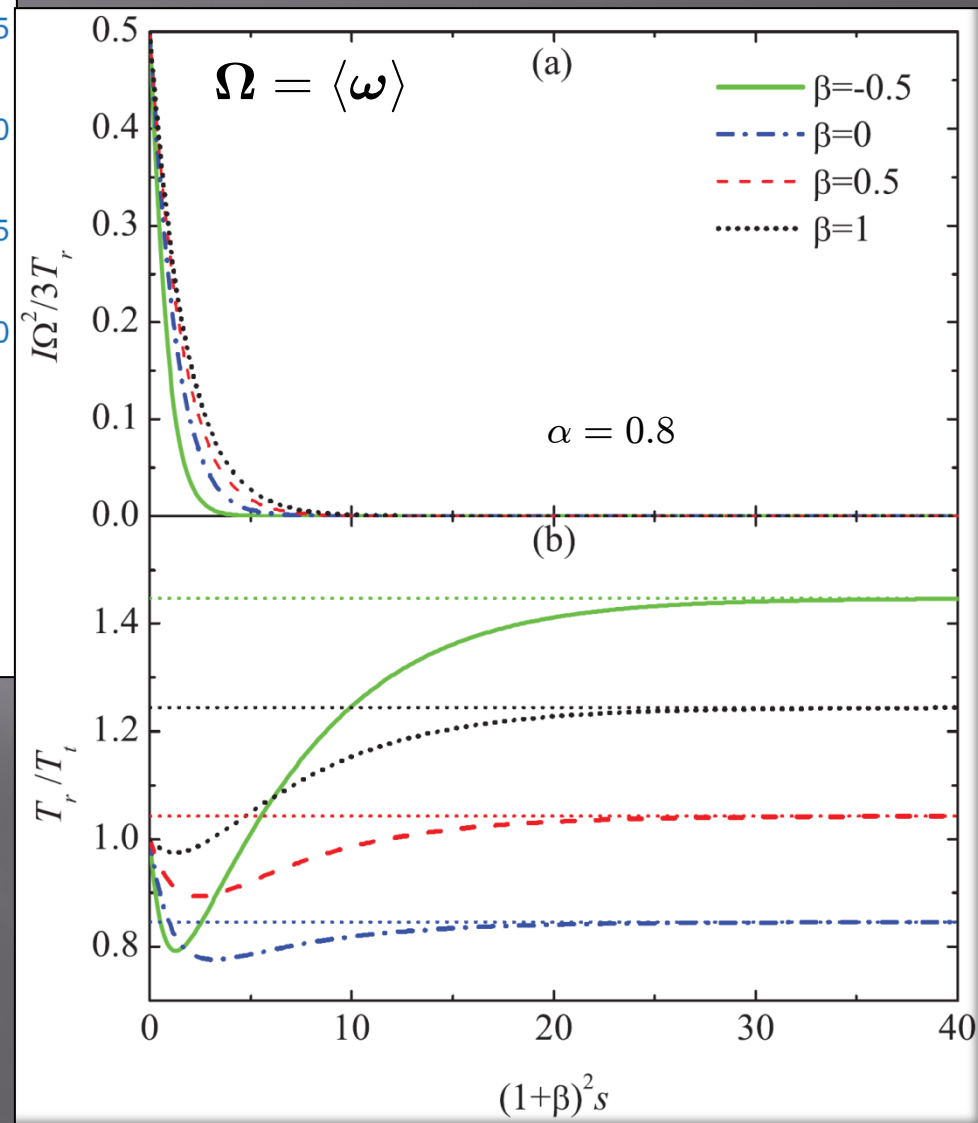
Boltzmann equation:

$$\partial_t f(\mathbf{r}, \mathbf{v}, \omega, t) + \mathbf{v} \cdot \nabla f(\mathbf{r}, \mathbf{v}, \omega, t) = J[\mathbf{r}, \mathbf{v}, \omega, t | f]$$

Inelastic+Rough collisions



N. V. Brilliantov, T. Pöschel, W. T. Kranz, and A. Zippelius, Phys. Rev. Lett. **98**, 128001 (2007)



G. M. Kremer, A. S., and V. Garzó, Phys. Rev. E **90**, 022205 (2014)

Inhomogeneous states. Hydrodynamic fields

Number density: $n(\mathbf{r}, t) = \int d\mathbf{v} \int d\omega f(\mathbf{r}, \mathbf{v}, \omega, t)$

Flow velocity: $\mathbf{u}(\mathbf{r}, t) = \frac{1}{n} \int d\mathbf{v} \int d\omega \mathbf{v} f(\mathbf{r}, \mathbf{v}, \omega, t)$

Temperature: $T(\mathbf{r}, t) = \frac{1}{2} [T_t(\mathbf{r}, t) + T_r(\mathbf{r}, t)]$
 $= \frac{1}{3n} \int d\mathbf{v} \int d\omega \left[m (\mathbf{v} - \mathbf{u})^2 + I\omega^2 \right] f(\mathbf{r}, \mathbf{v}, \omega, t)$

Hydrodynamic fluxes

$$\text{Pressure tensor: } \mathbf{P}(\mathbf{r}, t) = \int d\mathbf{v} \int d\omega (\mathbf{v} - \mathbf{u})(\mathbf{v} - \mathbf{u}) f(\mathbf{r}, \mathbf{v}, \omega, t)$$

$$\begin{aligned} \text{Heat flux: } \mathbf{q}(\mathbf{r}, t) &= \mathbf{q}_t(\mathbf{r}, t) + \mathbf{q}_r(\mathbf{r}, t) \\ &= \frac{1}{2} \int d\mathbf{v} \int d\omega \left[m(\mathbf{v} - \mathbf{u})^2 + I\omega^2 \right] \\ &\quad \times (\mathbf{v} - \mathbf{u}) f(\mathbf{r}, \mathbf{v}, \omega, t) \end{aligned}$$

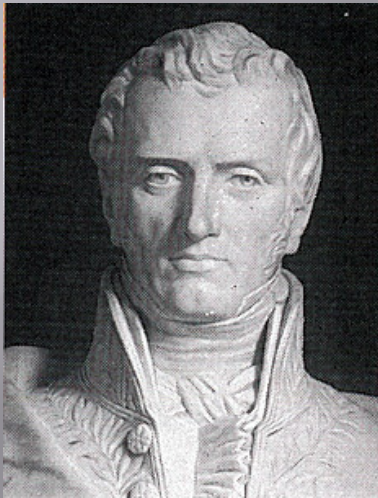
$$\begin{aligned} \text{Cooling rate: } \zeta(\mathbf{r}, t) &= \frac{I'_t}{2T} \zeta_t(\mathbf{r}, t) + \frac{I'_r}{2T} \zeta_r(\mathbf{r}, t) \\ &= -\frac{1}{6nT} \int d\mathbf{v} \int d\omega \left[m(\mathbf{v} - \mathbf{u})^2 + I\omega^2 \right] \\ &\quad \times J[\mathbf{r}, \mathbf{v}, \omega, t | f] \end{aligned}$$

Balance equations

$$\left. \begin{aligned} \mathcal{D}_t n + n \nabla \cdot \mathbf{u} &= 0 \\ \rho \mathcal{D}_t \mathbf{u} + \nabla \cdot \mathbf{P} &= 0 \\ \mathcal{D}_t T + \frac{1}{3n} (\nabla \cdot \mathbf{q} + \mathbf{P} : \nabla \mathbf{u}) &= -\zeta T \end{aligned} \right\}$$

$$(\mathcal{D}_t \equiv \partial_t + \mathbf{u} \cdot \nabla)$$

Navier-Stokes-Fourier constitutive equations



Claude-Louis Navier
(1785-1836)



George Gabriel Stokes
(1819-1903)



Jean-Baptiste Joseph Fourier
(1768-1830)

Navier-Stokes-Fourier constitutive equations

$$P_{ij} = n\tau_t T \delta_{ij} - \eta \left(\nabla_i u_j + \nabla_j u_i - \frac{2}{3} \delta_{ij} \nabla \cdot \mathbf{u} \right) - \eta_b \delta_{ij} \nabla \cdot \mathbf{u}$$

Shear viscosity

Bulk viscosity

$$\mathbf{q} = -\lambda \nabla T - \mu \nabla n$$

Dufour-like coefficient

Thermal conductivity

$$\zeta = \zeta^{(0)} - \xi \nabla \cdot \mathbf{u}$$

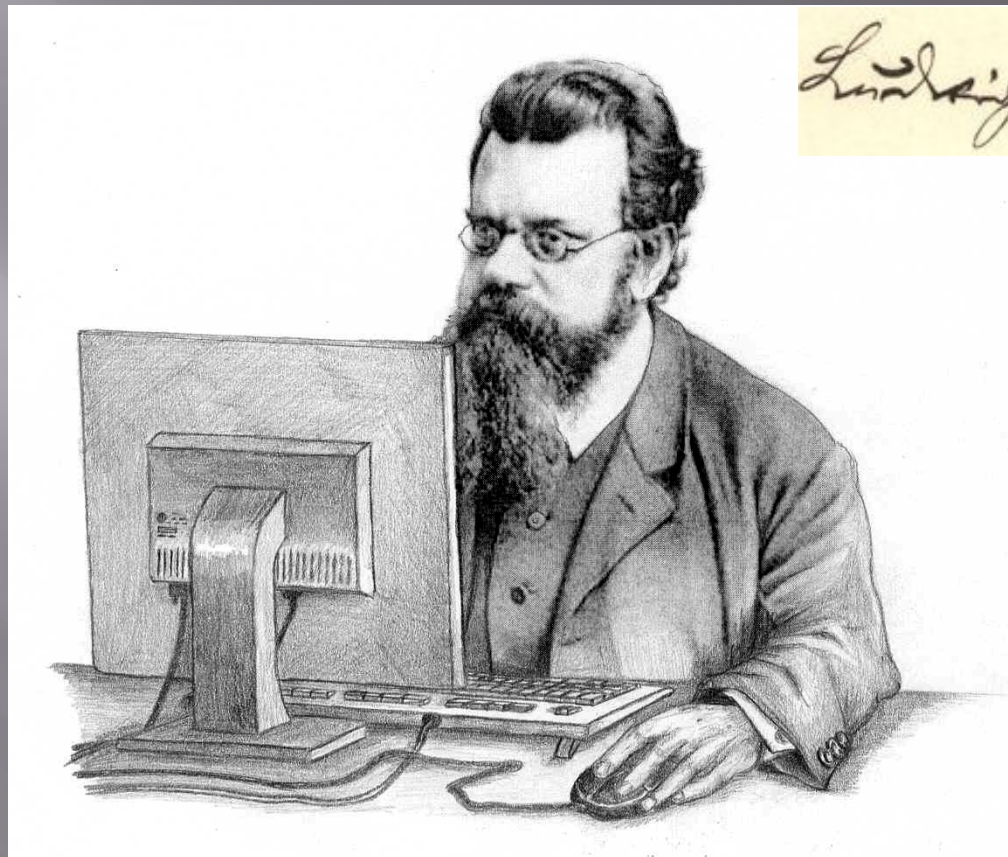
Cooling rate transport coefficient

Navier-Stokes-Fourier hydrodynamic equations

$$\mathcal{D}_t n + n \nabla \cdot \mathbf{u} = 0$$

$$\rho \mathcal{D}_t u_i + \nabla_i p^{(0)} = \nabla_j \left[\eta \left(\nabla_i u_j + \nabla_j u_i - \frac{2}{3} \delta_{ij} \nabla \cdot \mathbf{u} \right) + \eta_b \delta_{ij} \nabla \cdot \mathbf{u} \right]$$

$$\begin{aligned} \left(\mathcal{D}_t + \zeta^{(0)} \right) T + \frac{1}{3} T \tau_t \nabla \cdot \mathbf{u} &= \frac{1}{3n} \nabla \cdot (\lambda \nabla T + \mu \nabla n) \\ &+ \frac{1}{3n} \left[\eta \left(\nabla_i u_j + \nabla_j u_i - \frac{2}{3} \delta_{ij} \nabla \cdot \mathbf{u} \right) + \eta_b \delta_{ij} \nabla \cdot \mathbf{u} \right] \\ &\times \nabla_i u_j + T \xi \nabla \cdot \mathbf{u} \end{aligned}$$



Ludwig Boltzmann

(1844-1906)

(Cartoon by Bernhard Reischl, University of Vienna)

Boltzmann equation:

$$\partial_t f(\mathbf{r}, \mathbf{v}, \omega, t) + \mathbf{v} \cdot \nabla f(\mathbf{r}, \mathbf{v}, \omega, t) = J[\mathbf{r}, \mathbf{v}, \omega, t|f]$$

Inelastic+Rough collisions

Methodology: Chapman-Enskog method



Sydney Chapman
(1888-1970)



David Enskog
(1884-1947)

$$f = f^{(0)} + \epsilon f^{(1)} + \epsilon^2 f^{(2)} + \dots, \quad \epsilon \sim \nabla$$

$$\tilde{\alpha} = \frac{1+\alpha}{2}, \tilde{\beta} = \frac{1+\beta}{2} \frac{\kappa}{\kappa+1}$$

Explicit expressions

$$T_t^{(0)}/T = \tau_t = \frac{1}{1+\theta}, T_r^{(0)}/T = \tau_r = \frac{2\theta}{1+\theta}$$

$$\theta = \sqrt{1+h^2} + h, h \equiv \frac{(1+\kappa)^2}{2\kappa(\tilde{\alpha}+\tilde{\beta})^2} \left[\frac{1+\beta-\kappa}{2} \alpha^2 - (1-\beta^2) \frac{1-\kappa}{1+\kappa} \right]$$

ν HCS quantities $\zeta^{(0)}/\nu = \zeta^* = \frac{5}{12} \frac{1}{1+\theta}$

$$\theta = \sqrt{1+h^2} + h, h \equiv \frac{(1+\kappa)^2}{2\kappa(1+\beta)^2} \left[1 - \alpha^2 - (1-\beta^2) \frac{1-\kappa}{1+\kappa} \right]$$

$$\zeta^{(0)}/\nu = \zeta^* = \frac{5}{12} \frac{1}{1+\theta} \left[1 - \frac{\nu}{\zeta^{(0)}/\nu} = \zeta^* = \frac{5}{12} \frac{1}{1+\theta} \left[1 - \alpha^2 \frac{\theta+\kappa}{1+\kappa} - \beta^2 \frac{\theta+\kappa}{1+\kappa} \right] \right]$$

$\eta = (n\tau_t T/\nu)/(\nu_\eta^* - \frac{1}{2}\zeta^*)$

$$\eta_\theta = (n\tau_t \tau_r T/\nu)\gamma_E$$

NSF(coefficients) $\lambda = \tau_t \lambda_t + \tau_r \lambda_r, \lambda_t = \frac{5}{2} (\tau_t^2 T^2/m\nu)\gamma_{B_t}, \lambda_r = \frac{3}{2} (\tau_t \tau_r T^2/m\nu)\gamma_{B_r}$

$$\lambda = \tau_t \lambda_t + \tau_r \lambda_r, \lambda_t = \frac{5}{2} (\tau_t^2 T^2/m\nu)\gamma_{B_t}, \lambda_r = \frac{3}{2} (\tau_t \tau_r T^2/m\nu)\gamma_{B_r}$$

$\mu = \mu_t + \mu_r, \mu_t = \frac{5}{2} (\tau_t^2 T^2/m\nu)\gamma_{B_t}, \mu_r = \frac{3}{2} (\tau_t \tau_r T^2/m\nu)\gamma_{B_r}$

$$\mu = \mu_t + \mu_r, \mu_t = \frac{5}{2} (\tau_t^2 T^2/m\nu)\gamma_{B_t}, \mu_r = \frac{3}{2} (\tau_t \tau_r T^2/m\nu)\gamma_{B_r}$$

$\xi = \frac{1}{2} (\tau_t \xi_t + \tau_r \xi_r) = \gamma_E \Xi_t, \xi_t = \frac{5}{8} \tau_t \left[1 - \alpha^2 + (1 - \beta^2) \frac{1+\beta}{1+\kappa} \right] \left(\frac{1+\beta}{1+\kappa} \right)^2$

$$\xi = \frac{1}{2} (\tau_t \xi_t + \tau_r \xi_r) = \gamma_E \Xi_t, \xi_t = \frac{5}{8} \tau_t \left[1 - \alpha^2 + (1 - \beta^2) \frac{1+\beta}{1+\kappa} \right] \left(\frac{1+\beta}{1+\kappa} \right)^2$$

$\nu_\eta^* = (\tilde{\alpha} + \tilde{\beta})(2 - \tilde{\alpha} - \tilde{\beta}) \pm \frac{\beta^2 \theta}{6\kappa} + (1 - \beta^2) \left(1 + \frac{1}{3} \frac{\theta - 5}{1 + \kappa} \right)$

$$\nu_\eta^* = (\tilde{\alpha} + \tilde{\beta})(2 - \tilde{\alpha} - \tilde{\beta}) \pm \frac{\beta^2 \theta}{6\kappa} + (1 - \beta^2) \left(1 + \frac{1}{3} \frac{\theta - 5}{1 + \kappa} \right)$$

Auxiliary quantities $\gamma_{A_t} = \frac{Z_r - Z_t - 2\zeta^*}{(Y_t - 2\zeta^*)(Z_r - 2\zeta^*) - Y_r Z_t}$

$$\gamma_{A_t} = \frac{Z_r - Z_t - 2\zeta^*}{(Y_t - 2\zeta^*)(Z_r - 2\zeta^*) - Y_r Z_t}$$

$\gamma_{A_r} = \frac{Y_t - Y_r - 2\zeta^*}{(Y_t - 2\zeta^*)(Z_r - 2\zeta^*) - Y_r Z_t}$

$$\gamma_{A_r} = \frac{Y_t - Y_r - 2\zeta^*}{(Y_t - 2\zeta^*)(Z_r - 2\zeta^*) - Y_r Z_t}$$

$\Xi_t = \frac{5}{8} \tau_t \left[1 - \alpha^2 + (1 - \beta^2) \frac{1+\beta}{1+\kappa} \right] \left(\frac{1+\beta}{1+\kappa} \right)^2$

$$\Xi_t = \frac{5}{8} \tau_t \left[1 - \alpha^2 + (1 - \beta^2) \frac{1+\beta}{1+\kappa} \right] \left(\frac{1+\beta}{1+\kappa} \right)^2$$

$\Xi_r = \frac{5}{8} \tau_r \frac{1+\beta}{1+\kappa} \left[\frac{\theta-2}{3} (1 - \beta) \right]$

$$\Xi_r = \frac{5}{8} \tau_r \frac{1+\beta}{1+\kappa} \left[\frac{\theta-2}{3} (1 - \beta) \right]$$

$\Xi = \frac{5}{16} \tau_t \tau_r \left[1 - \alpha^2 + (1 - \beta^2) \frac{1+\beta}{1+\kappa} \right]$

$$\Xi = \frac{5}{16} \tau_t \tau_r \left[1 - \alpha^2 + (1 - \beta^2) \frac{1+\beta}{1+\kappa} \right]$$

$Z_r = \frac{5}{6} (\tilde{\alpha} + \tilde{\beta}) + \frac{5}{18} \frac{\beta}{\kappa} (7 - 3\frac{\tilde{\beta}}{\kappa} - 6\tilde{\beta} - 4\tilde{\alpha})$

$$Z_r = \frac{5}{6} (\tilde{\alpha} + \tilde{\beta}) + \frac{5}{18} \frac{\beta}{\kappa} (7 - 3\frac{\tilde{\beta}}{\kappa} - 6\tilde{\beta} - 4\tilde{\alpha})$$

$\gamma_{A_t} = \frac{Z_r - Z_t - 2\zeta^*}{(Y_t - 2\zeta^*)(Z_r - 2\zeta^*) - Y_r Z_t}$

$$\gamma_{A_t} = \frac{Z_r - Z_t - 2\zeta^*}{(Y_t - 2\zeta^*)(Z_r - 2\zeta^*) - Y_r Z_t}$$

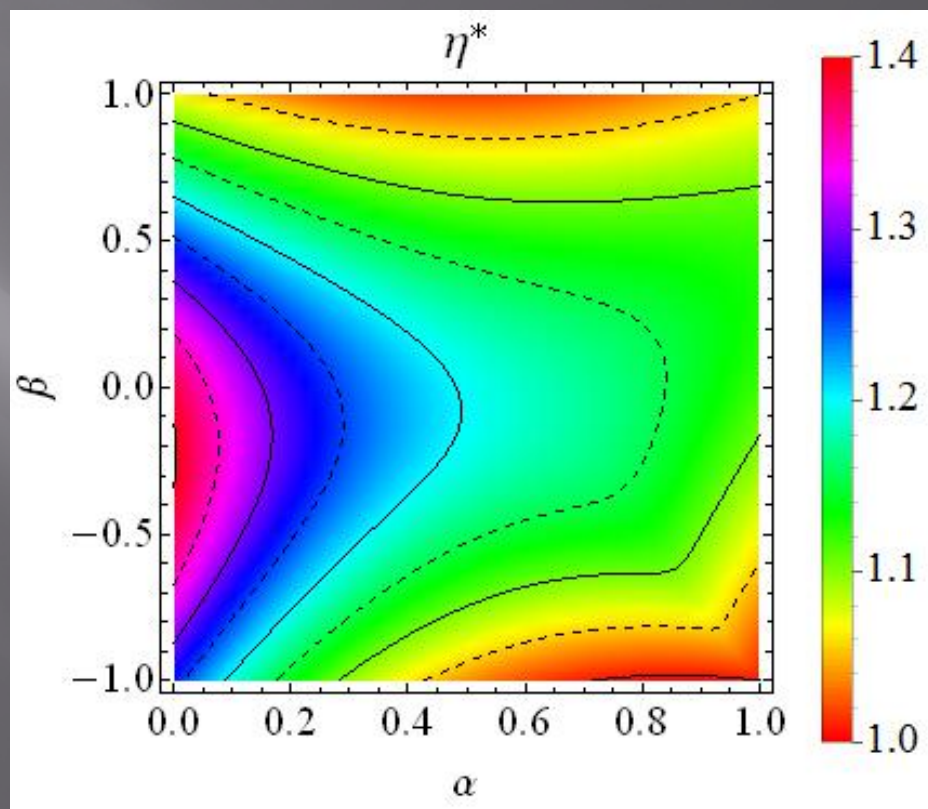
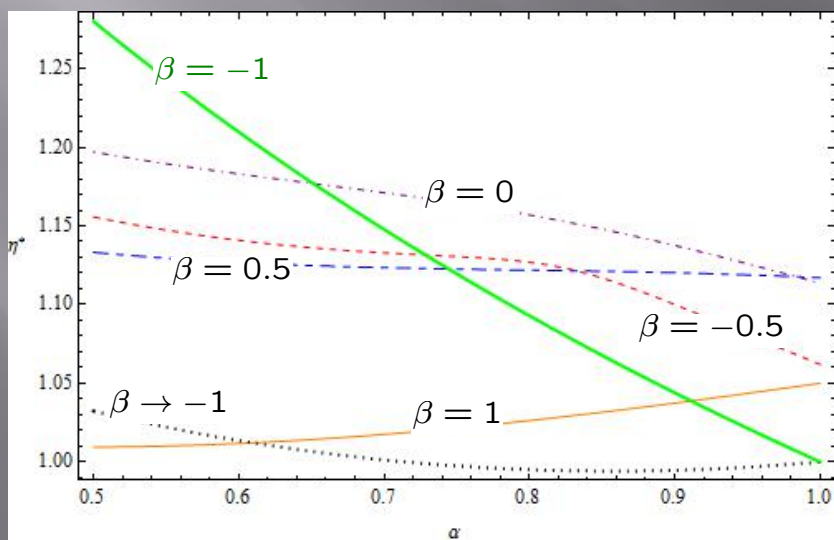
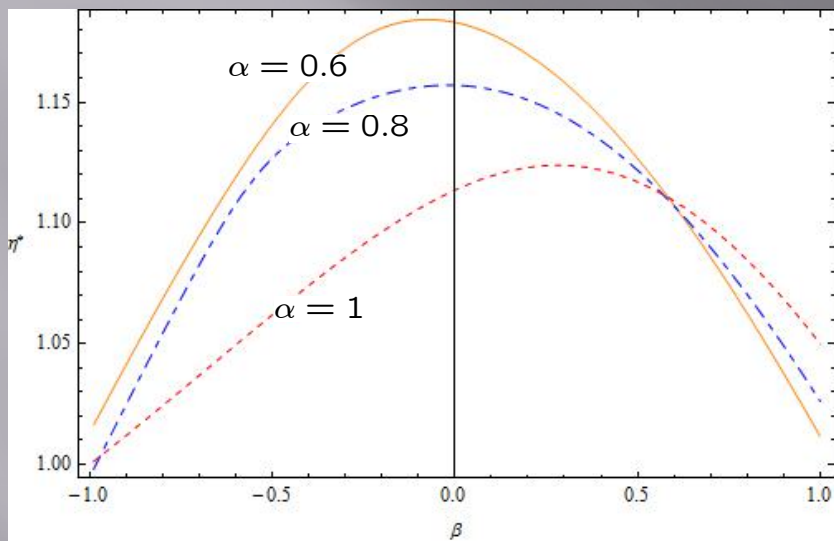
Special limiting cases

Quantity	Pure smooth ($\beta = -1$)	Quasi-smooth limit ($\beta \rightarrow -1$)	Perfectly rough and elastic ($\alpha = \beta = 1$)
η^*	$\frac{24}{(1 + \alpha)(13 - \alpha)}$	$\frac{24}{(1 + \alpha)(19 - 7\alpha)}$	$\frac{6(1 + \kappa)^2}{6 + 13\kappa}$
η_b^*	0	$\frac{8}{5(1 - \alpha^2)}$	$\frac{(1 + \kappa)^2}{10\kappa}$
λ^*	$\frac{64}{(1 + \alpha)(9 + 7\alpha)}$	$\frac{48}{25(1 + \alpha)}$	$\frac{12(1 + \kappa)^2 (37 + 151\kappa + 50\kappa^2)}{25 (12 + 75\kappa + 101\kappa^2 + 102\kappa^3)}$
μ^*	$\frac{1280(1 - \alpha)}{(1 + \alpha)(9 + 7\alpha)(19 - 3\alpha)}$	0	0
ξ	0	0	0

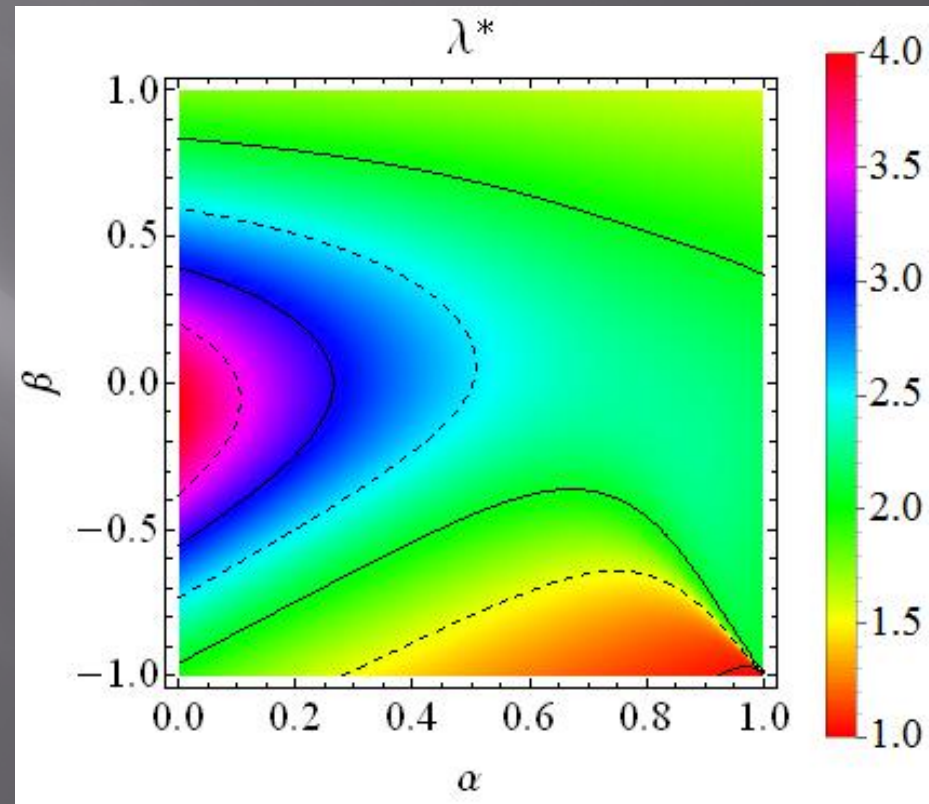
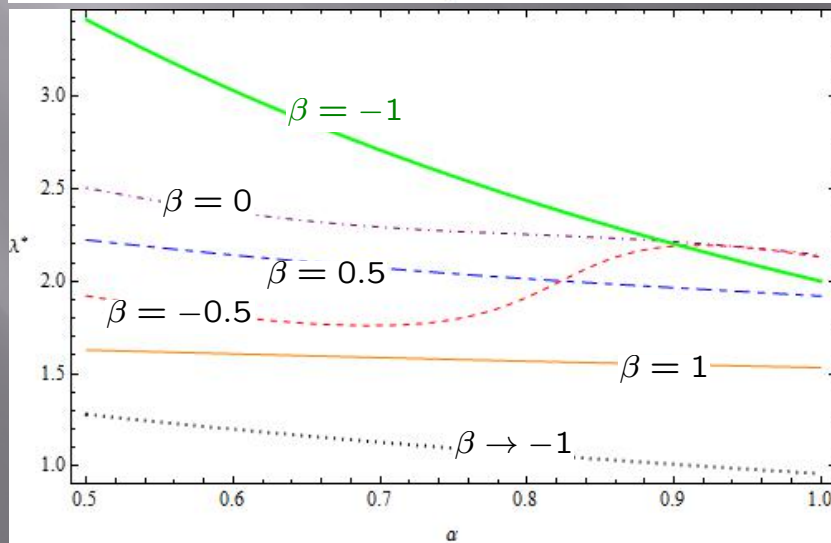
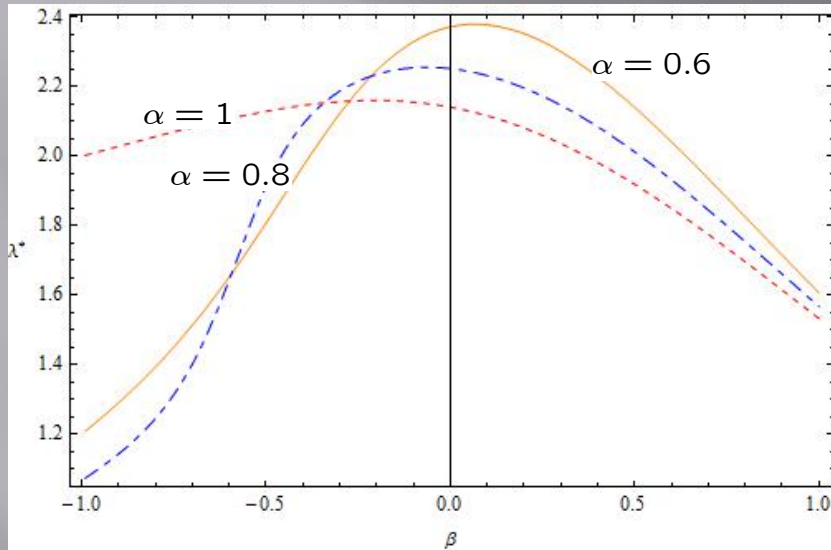
Brey, Dufty, Kim, Santos
(1998)

Pidduck
(1922)

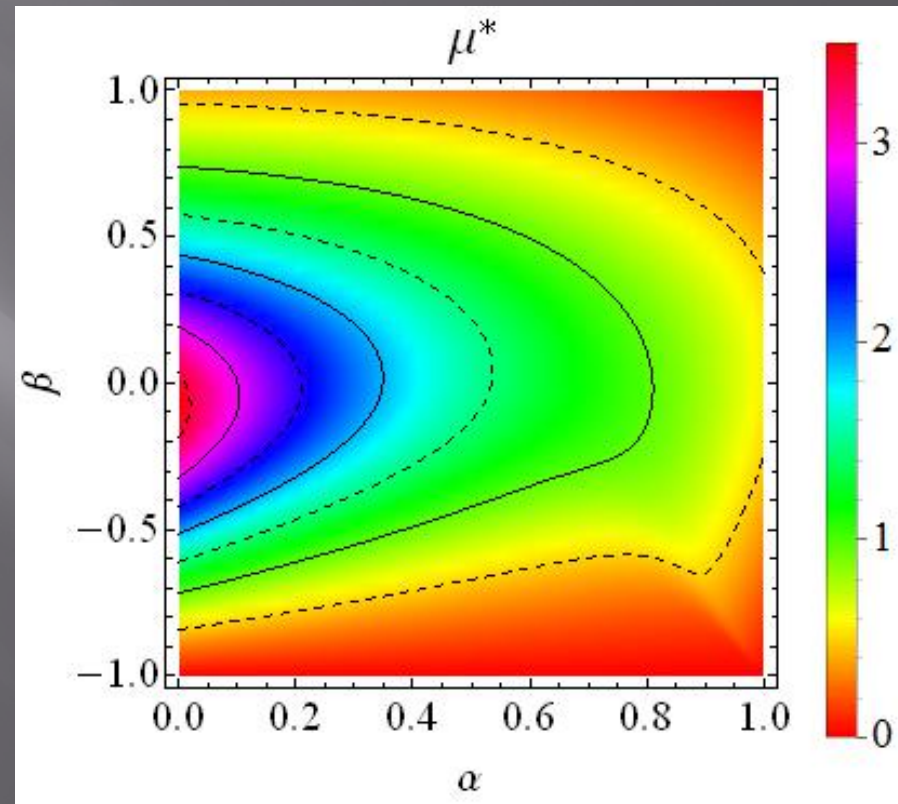
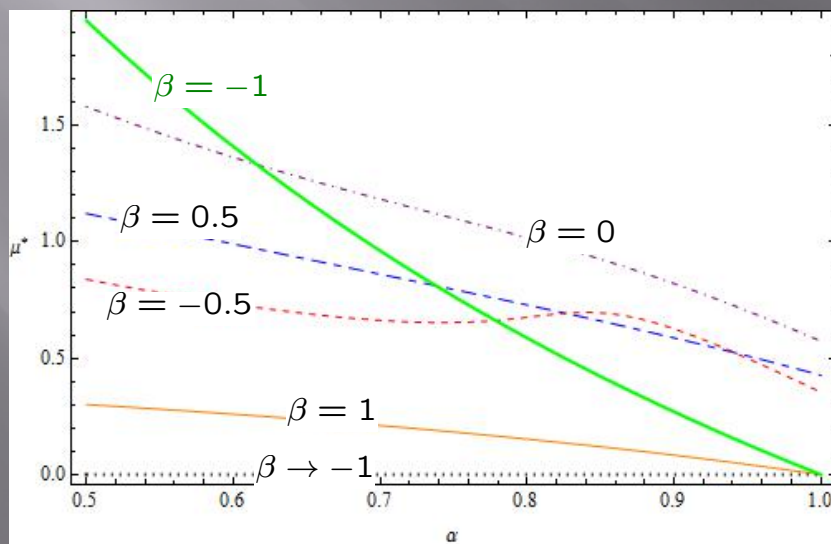
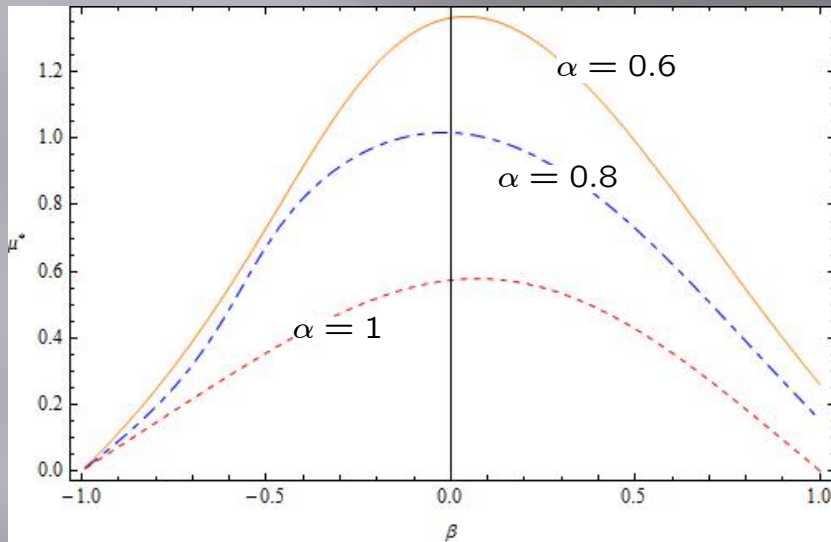
Shear viscosity



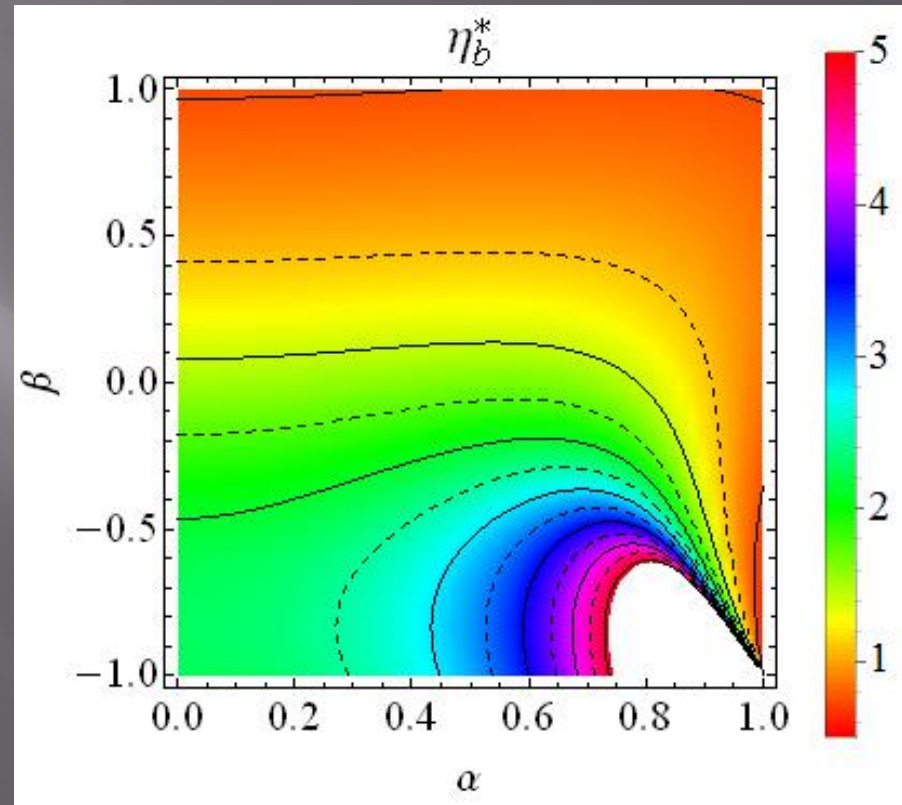
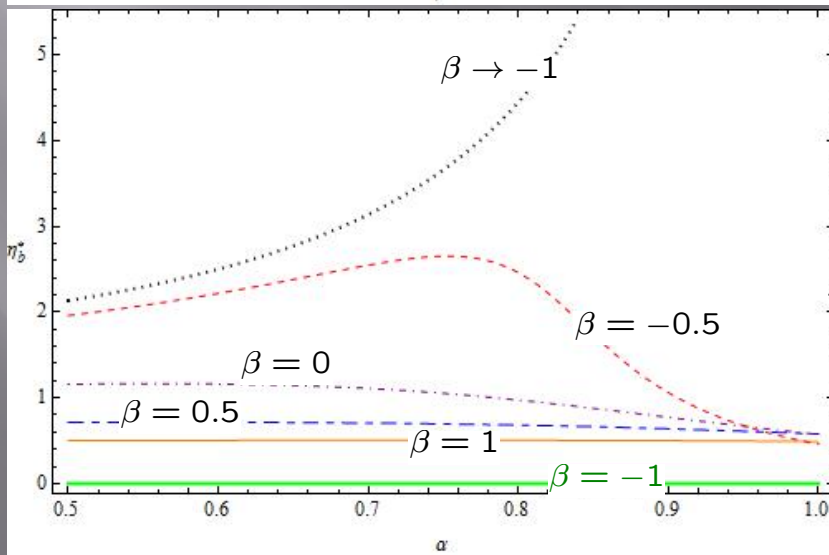
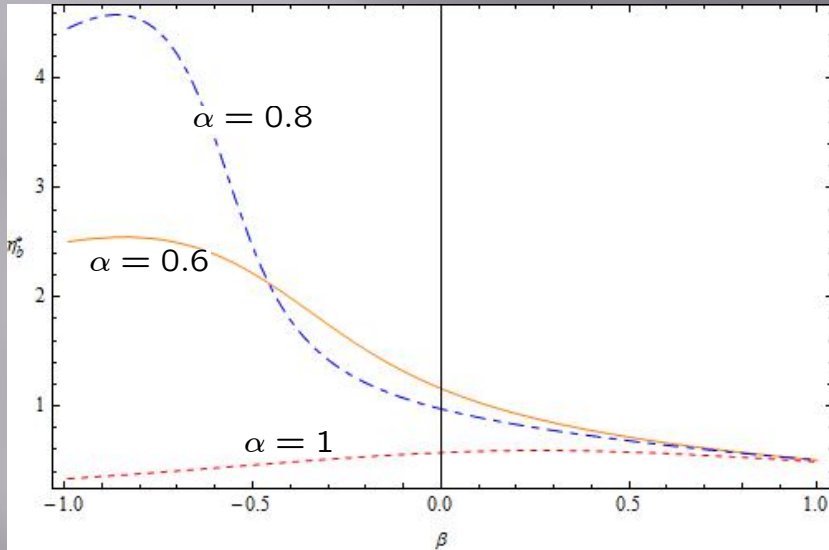
Thermal conductivity



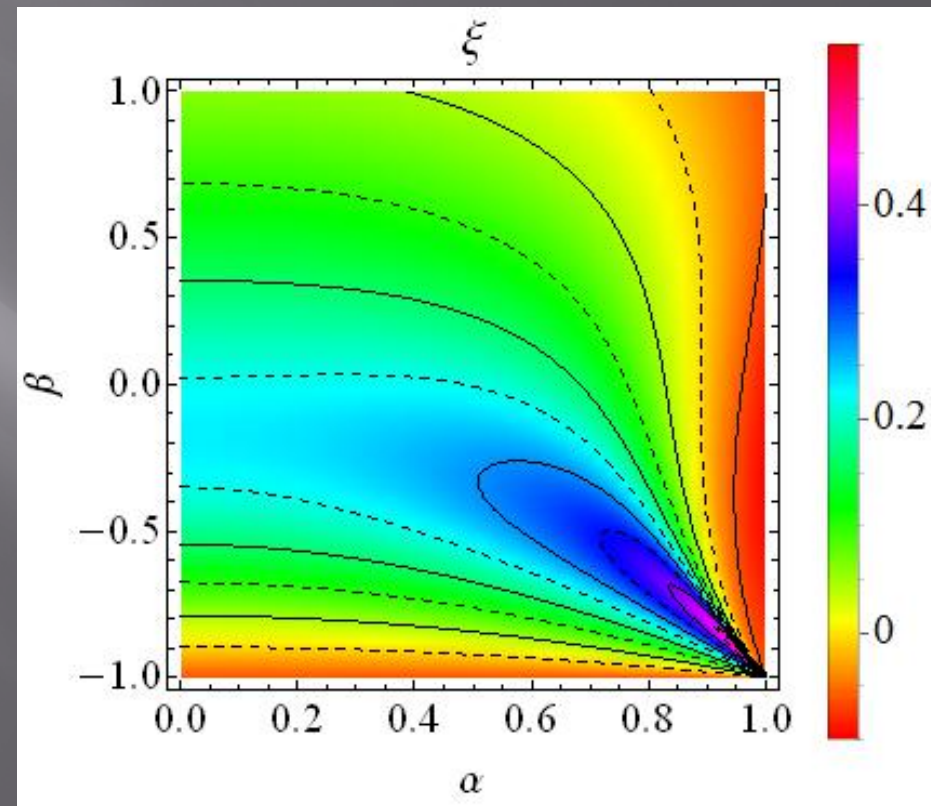
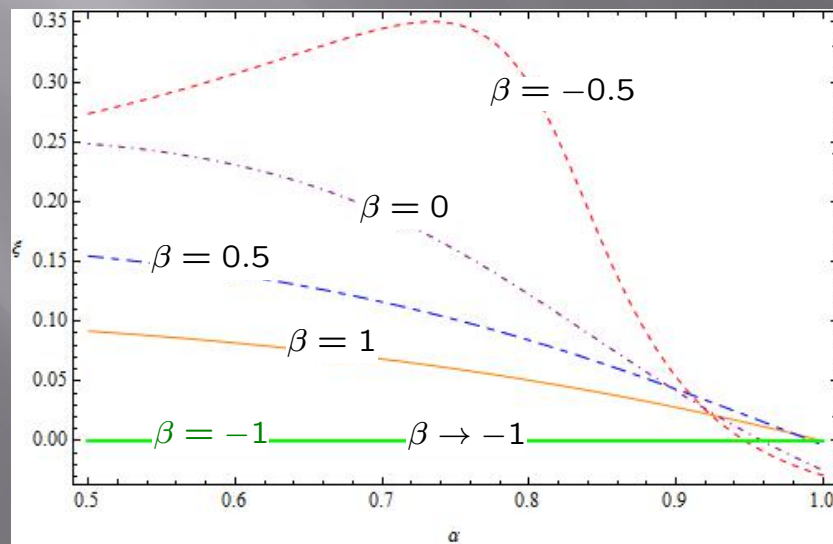
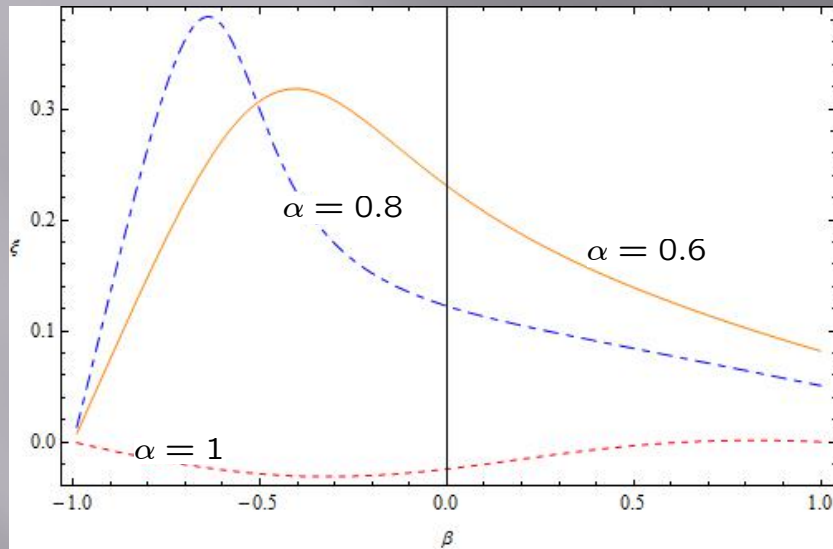
Dufour-like coefficient



Bulk viscosity



Cooling rate coefficient



Outline of the talk

- ▣ 0. Collision rules for inelastic rough hard spheres
- ▣ 1. Navier-Stokes-Fourier transport coefficients
- ▣ 2. Stability analysis
- ▣ 3. Conclusions

Instability of the HCS

J. Fluid Mech. (2013), vol. 729, pp. 484–495. © Cambridge University Press 2013
doi:10.1017/jfm.2013.328 484

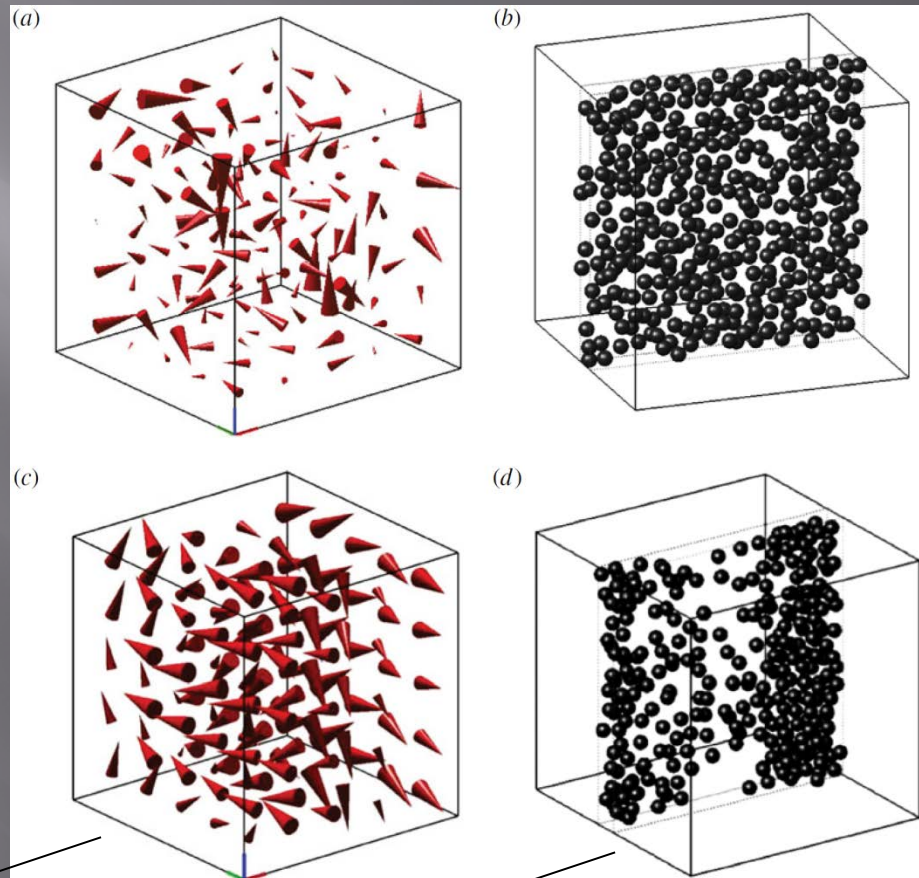
Dual role of friction in granular flows: attenuation versus enhancement of instabilities

Peter P. Mitrano, Steven R. Dahl, Andrew M. Hilger, Christopher J. Ewasko
and Christine M. Hrenya†

$$\alpha = 0.7, \quad \beta = -0.7$$

volume fraction $\phi = 0.3$

$$L/\sigma = 10$$



Vortices

Clustering

Nonlinear NSF hydrodynamic equations

$$\mathcal{D}_t n + n \nabla \cdot \mathbf{u} = 0$$

$$\rho \mathcal{D}_t u_i + \nabla_i p^{(0)} = \nabla_j \left[\eta \left(\nabla_i u_j + \nabla_j u_i - \frac{2}{3} \delta_{ij} \nabla \cdot \mathbf{u} \right) + \eta_b \delta_{ij} \nabla \cdot \mathbf{u} \right]$$

$$\begin{aligned} \left(\mathcal{D}_t + \zeta^{(0)} \right) T + \frac{1}{3} T \tau_t \nabla \cdot \mathbf{u} &= \frac{1}{3n} \nabla \cdot (\lambda \nabla T + \mu \nabla n) \\ &+ \frac{1}{3n} \left[\eta \left(\nabla_i u_j + \nabla_j u_i - \frac{2}{3} \delta_{ij} \nabla \cdot \mathbf{u} \right) + \eta_b \delta_{ij} \nabla \cdot \mathbf{u} \right] \\ &\times \nabla_i u_j + T \xi \nabla \cdot \mathbf{u} \end{aligned}$$

Linear stability analysis

$$\left. \begin{aligned} n(\mathbf{r}, t) &= n_H [1 + \delta n^*(\mathbf{r}, t)] \\ \mathbf{u}(\mathbf{r}, t) &= \mathbf{u}_H + v_H(t) \delta \mathbf{u}^*(\mathbf{r}, t) \\ T(\mathbf{r}, t) &= T_H(t) [1 + \delta T^*(\mathbf{r}, t)] \end{aligned} \right\} \delta y_\alpha(\mathbf{r}, t), \quad \alpha = 1, \dots, 5$$

Fourier-Laplace transform:

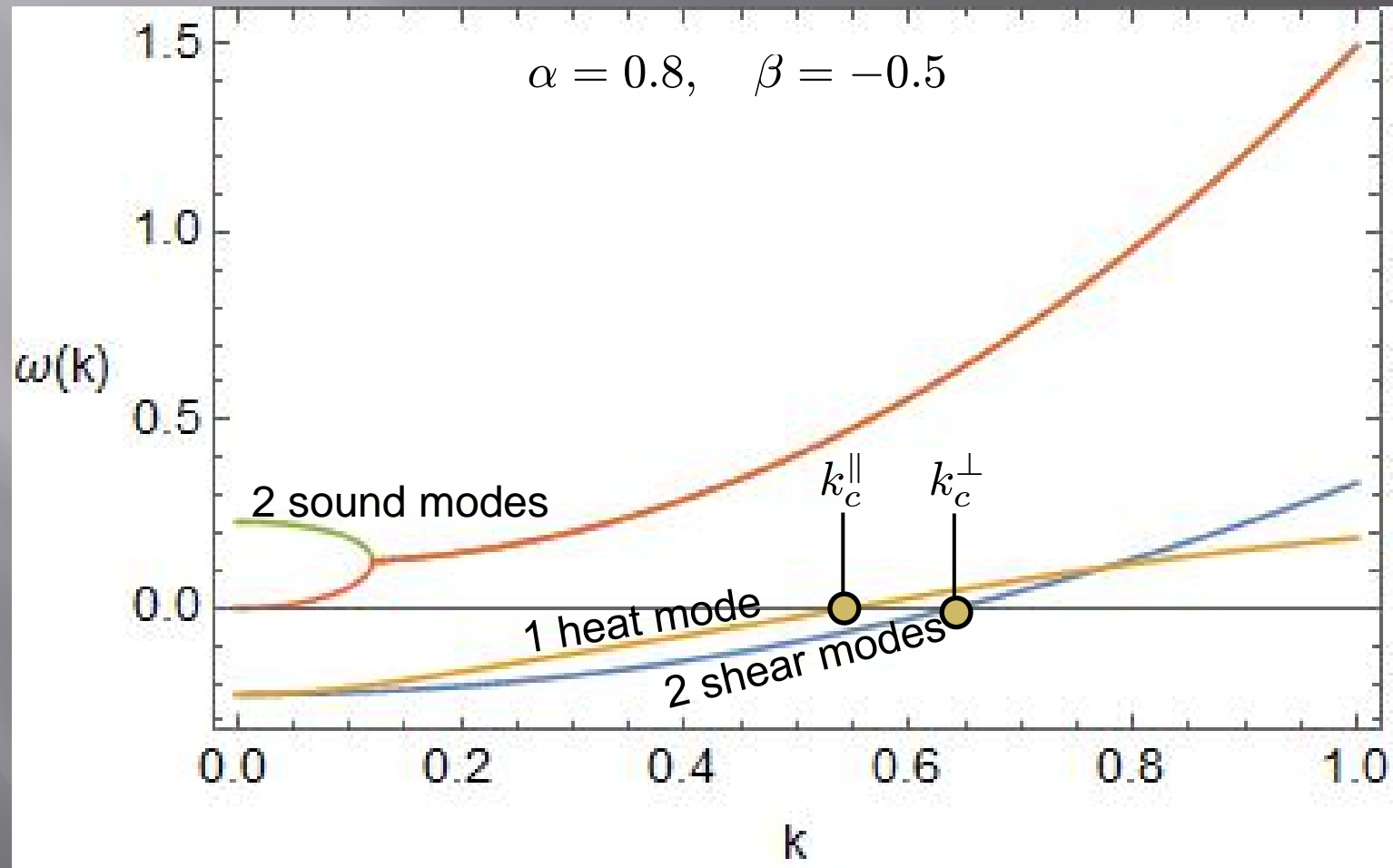
$$\delta y_\alpha(\mathbf{r}, t) = \delta y_{\alpha; \mathbf{k}, \omega} e^{i\mathbf{k} \cdot \mathbf{r}^*} e^{-\omega(k)s} \left[\mathbf{r}^* \equiv \frac{\mathbf{r}}{\text{m.f.p.}}, \quad s \equiv \frac{1}{2} \int_0^t dt' \nu_H(t') \right]$$

Characteristic equation:

$$\det [\mathbf{M}(k) - \omega(k)\mathbf{I}] = 0 \Rightarrow \text{Dispersion relation}$$

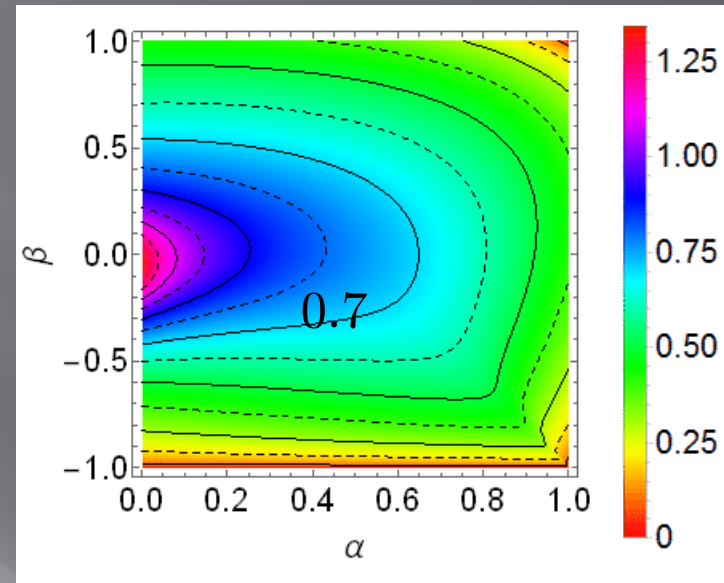
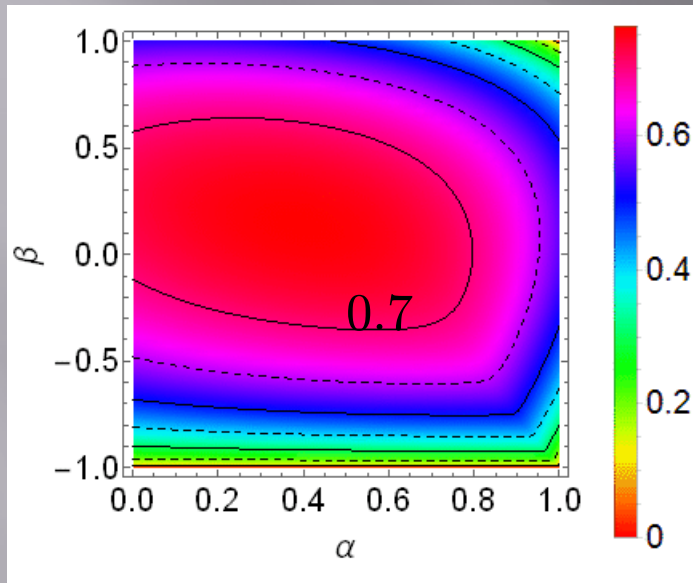
$$\omega(k) < 0 \Rightarrow \text{Instability}$$

Dispersion relations

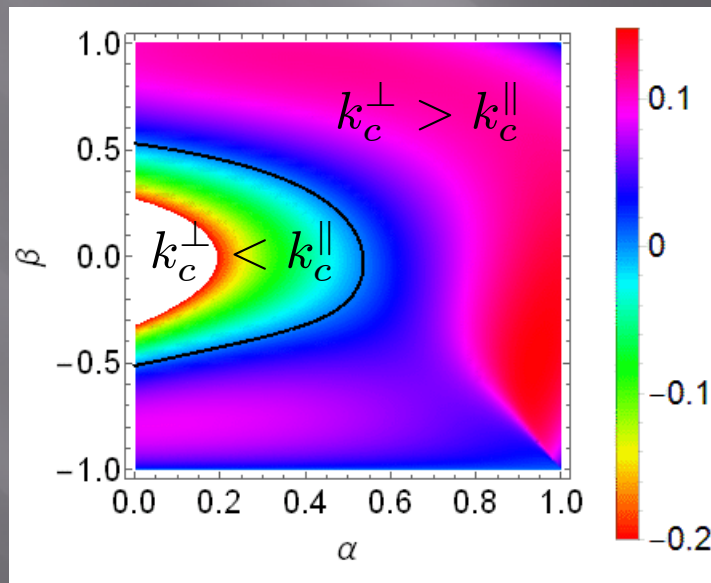


$$k_c^\perp(\alpha, \beta) = \sqrt{2\zeta^*/\eta^*}$$

$$k_c^\parallel(\alpha, \beta) = \sqrt{8\zeta^*/5(\lambda^* - \mu^*)}$$



The shear modes (vortices) are more unstable than the heat mode (clusters), except for high inelasticity and medium roughness

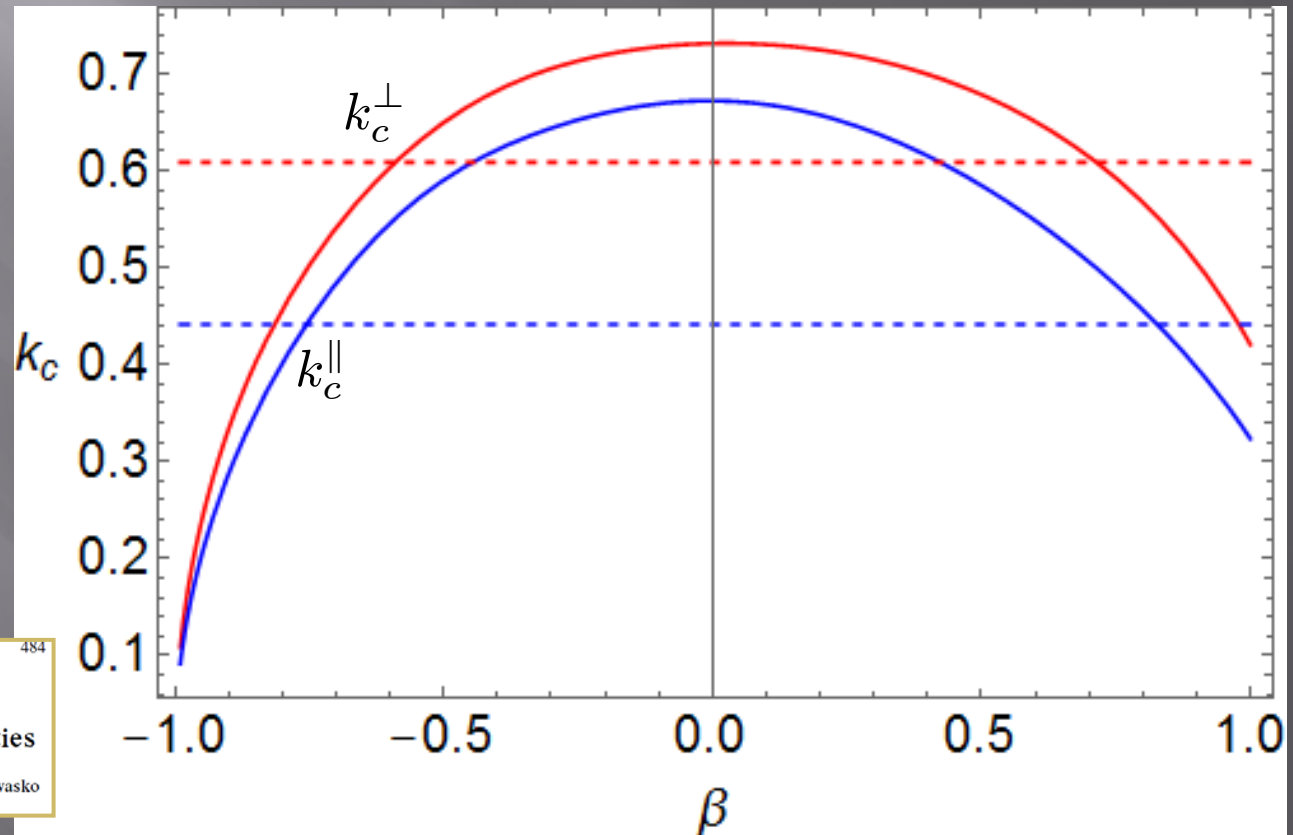


$$k_c^\perp(\alpha, \beta) - k_c^\parallel(\alpha, \beta)$$

Comparison with the pure smooth case

Medium roughness enhances instabilities, while small and high levels of roughness attenuate it

$$\alpha = 0.7$$



J. Fluid Mech. (2013), vol. 729, pp. 484–495. © Cambridge University Press 2013
doi:10.1017/jfm.2013.328

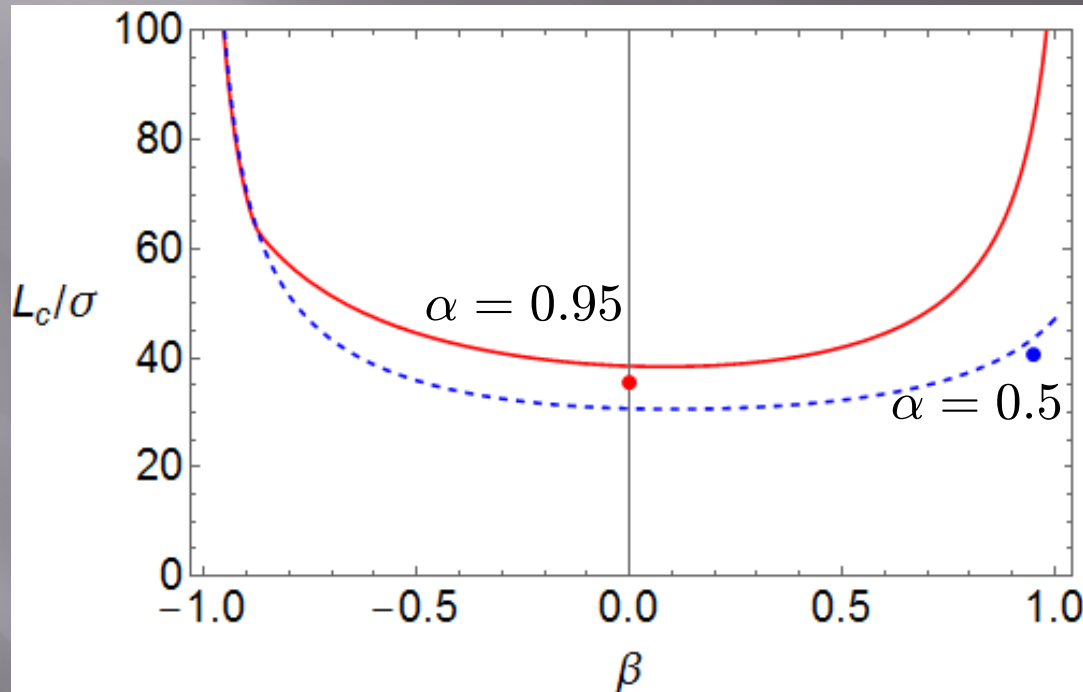
484

Dual role of friction in granular flows:
attenuation versus enhancement of instabilities

Peter P. Mitrano, Steven R. Dahl, Andrew M. Hilger, Christopher J. Ewasko
and Christine M. Hrenya†

Comparison with preliminary MD simulations

volume fraction $\phi = 0.05$



(MD points, courtesy of Peter Mitrano)

Outline of the talk

- ▣ 0. Collision rules for inelastic rough hard spheres
- ▣ 1. Navier-Stokes-Fourier transport coefficients
- ▣ 2. Stability analysis
- ▣ 3. Conclusions

Conclusions

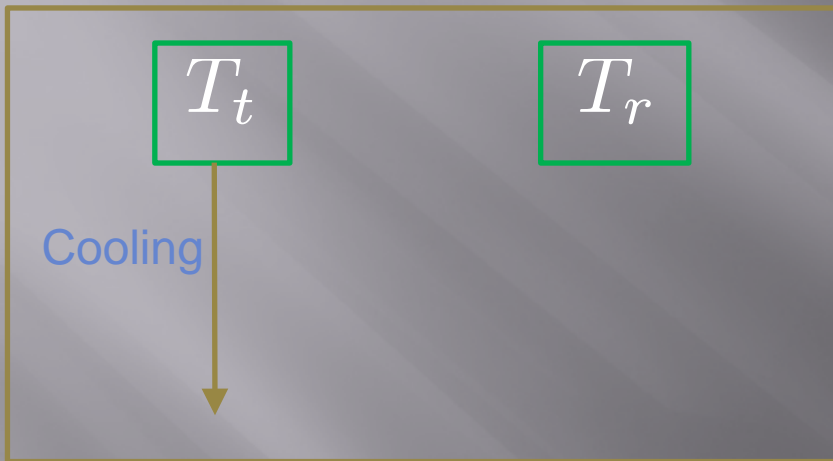
- ▣ Roughness induces two extra transport coefficients (η_b, ξ), not present in the case of a (dilute) gas of smooth spheres.
- ▣ Typically, at fixed α the coefficients have a maximum at an intermediate value of β .
- ▣ In general, the dependence of the coefficients on α is weaker than in the case of smooth spheres.
- ▣ Medium roughness enhances instabilities; small and large levels of roughness attenuate it.

Thank you for your attention!



Origin of the singular behavior in the quasi-smooth limit

$$\beta = -1$$



$$\beta \gtrsim -1$$

